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# Mechanical behaviors of Fe<sub>3</sub>Al with vanadium addition<sup>®</sup>

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[Abstract] The effect of V on mechanical property of Fe<sub>3</sub>Al-based ordered alloy was studied. The results show that V can refine grains which improves strength and plasticity of Fe<sub>3</sub>Al. As contrasted with transgranular fracture of Fe<sub>3</sub>Al at room temperature, the Fe<sub>3</sub>Al containing V has intergranular and transgranular cleavage mixed fracture mode which is gradually changed into void fracture as tensile temperature increases. The DO<sub>3</sub>-ordered Fe<sub>3</sub>Al with V has maximum tensile strength at 700  $^{\circ}$ C which is much higher about 200  $^{\circ}$ C than that of DO<sub>3</sub>-ordered Fe<sub>3</sub>Al without V.

[Key words] DO<sub>3</sub>-ordered Fe<sub>3</sub>Al; vanadium; mechanical properties

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#### 1 INTRODUCTION

The iron aluminide Fe<sub>3</sub>Al occurs within the range of 24% ~ 32% (mole fraction) aluminum. It has three possible structures: BCC, which is stable at about 760 °C, imperfect B₂-order structure at 540~ 760 °C, and DO<sub>3</sub>-order structure which is stable below the critical temperature of 540 °C. DO<sub>3</sub>-ordered Fe<sub>3</sub>Al alloys have excellent oxidation resistance, good high temperature strength, relatively low density and cost. These advantages have led to consideration for structure applications at elevated temperatures<sup>[1]</sup>. However, the lack of ductility at room temperature and a sharp drop in strength above 600 °C have been major obstacles to their engineering applications. Recently many research reports showed that alloying elements can improve their mechanical properties. For example, addition of alloying elements such as Cr, Mn and Ce can improve their ductility at room temperature<sup>[2~7]</sup>, and significant increase of yield strength of the alloys above 600 °C results from adding Cr, Mo, Ni or Si. The purpose of this paper is to report the effect of V on the mechanical properties of DO<sub>3</sub>-ordered Fe<sub>3</sub>Al at room and elevated temperatures.

#### 2 EXPERIMENTAL

## 2. 1 Materials and method

Two DO<sub>3</sub>-ordered Fe<sub>3</sub>Al alloys were studied. They were Fe 28% Al (mole fraction) and Fe 28% Al-1.5% V (mole fraction). The alloys were melted in a vacuum induction furnace and cast into moulds. After homogenized at 950 °C for 4 h, the alloys were hot-rolled at 950 °C and warm-rolled at 650 °C from 7 mm to 0.7 mm. The rolled sheets were cleaned in a

solution of 95%  $\rm H_2O$  and 5% hydrochloric acid to remove surface oxide layer. Tensile samples with a gauge section of 0.7 mm  $\times$  5 mm  $\times$  20 mm punched from the sheet and then heat treated for 1 h in air at 800 °C for recrystallization and at 450 °C for DO3 ordering. The tensile samples were tested at 25  $\sim$  850 °C in air at a strain rate of 3.3  $\sim$  5  $\times$  10  $^{-2}$  s  $^{-1}$  on an LX-250 kg tensile machine. The fracture surfaces were examined by DXS-X2 scanning electron microscope (SEM).

## 2. 2 Mechanical properties

Tensile test results are shown in Fig. 1. It is known from Fig. 1 that both alloys have the characteristic of brittle material at room temperature, but Fe<sub>3</sub>Al has lower strength than Fe<sub>3</sub>Al with V. The DO<sub>3</sub>-ordered Fe<sub>3</sub>Al has the highest tensile strength at about 500 °C. Its tensile strength increased with increasing temperature below 500 °C and decreased greatly with increasing temperature above 500 °C. Necking occured in the Fe<sub>3</sub>Al tensile samples at about 600 °C. Addition of V could improve the strength of Fe<sub>3</sub>Al at room temperature. The tensile samples of Fe<sub>3</sub>Al with V showed that the tensile strength increases when the temperature is up to 700 °C. Its ductility increased with temperature. The change of yield strength was more complicated for the alloys. The Fe<sub>3</sub>Al containing V had change in yield strength similar to Fe<sub>3</sub>Al, as shown in Fig. 1(b), but its yield strength peak is about 200 °C higher than that of the alloy without V addition. This phenomenon was explained by order change in the alloys. Stoloff et al<sup>[8]</sup> reported that the unusual strength-temperature relation was connected with degree of ordering in DO<sub>3</sub> Fe<sub>3</sub>Al. The increase of yield strength was related exactly to the change in degree of ordering from 0.8 to

0 as the temperature increases from about 350 °C to 550 °C. The increase of yield strength responds to super dislocations within the range of temperatures and ordinary unit dislocations above about 550 °C. The yield strength peak was observed at the position of transition from unit dislocations to super dislocations. Mekhrabov et al's research result showed that V raised the temperature at which DO3-ordered structure exists<sup>[9]</sup>. Because V raised DO<sub>3</sub>-existing temperature, the increase of yield strength related to a mechanism of super dislocations could been retained at higher temperature, which made unusual strengthtemperature relation of DO<sub>3</sub> Fe<sub>3</sub>Al be at above 550 °C. SEM observation in our experiment showed that V element distributed uniformly in the alloy and the gain sizes were smaller in the alloy with V than that in the alloy without V. It is suggested that V addition improves mechanical properties of DO<sub>3</sub>-ordered Fe<sub>3</sub>Al alloy.

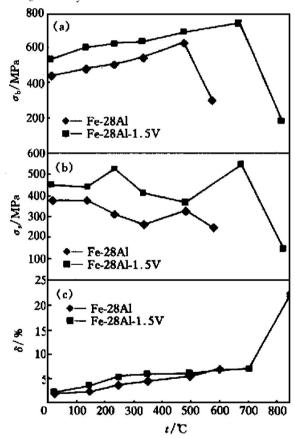


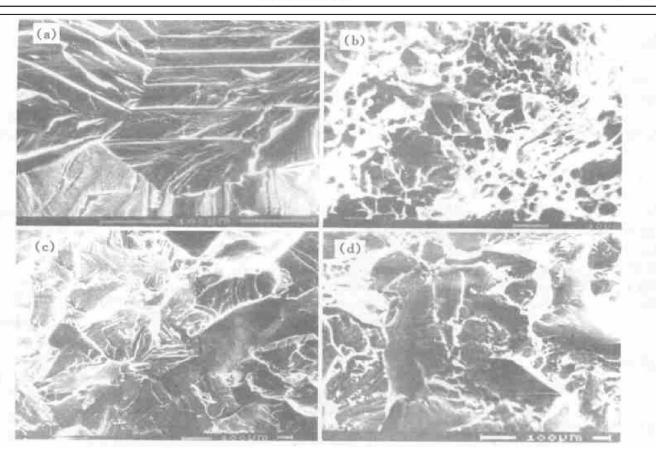
Fig. 1 Mechanical property—temperature curves of alloys

## 2. 3 Fracture mode

The tensile fracture modes of alloys were observed by SEM. The results showed the differences in fractures, crack shapes, and distribution in the alloy with and without V, as shown in Fig. 2. DO<sub>3</sub>-ordered Fe<sub>3</sub>Al without V has transgranular cleavage fracture mode at room temperature. It can be seen from Fig. 2(a) that cleavage planes are large and there are many parallel secondary transgranular cracks from gain boundaries to inside grains, indicating easy

crack propagation during the fracture of Fe-28Al alloy. As temperature increased to 350 °C, the fine nests occured near grain boundaries. The fracture mode transformed from transgranular cleavage to void at 500 °C, as shown in Fig. 2(b). On the other hand, the DO<sub>3</sub>-ordered alloy with V had transgranular cleavage intergranular fracture mode at room temperature, as shown in Fig. 2(c). Its cleavage planes are small and consisted of small cleavage steps and ripple ridges, which suggests higher cleavage strength in the alloy with V, compared with the alloy without V. The proportion of intergranular fracture increased with temperature in the alloy with V. The fine voids occurred at grain boundaries as temperature increased to 500 °C, as shown in Fig. 2(d) and complete void fracture took place at 700 °C. The optical observation of crack propagation was also done under tension. The cracks in the alloy with V additive appeared zigzag and there are a lot of slender slip lines around the tip of crack while the crack looked rather straight and no obvious trace of plastic deformation at crack tip was found in the alloy without V. It is indicated that the addition of V can refine grain and then improve the mechanical property of the alloy and is suggested that crack propagation is somehow retarded due to plastic deformation arising from the emission of dislocations at crack tip if Fe<sub>3</sub>Al alloy contains V additive.

In general, there are two types of fracture in alloys: brittleness and plasticity. The brittle fracture can be transgranular or intergranular according to related value of cleavage strength to boundary strength. If cleavage strength is lower than grain boundary strength, the cleavage fracture occured, and vice versa. The trend of intergranular fracture is intensified with temperature. During tension, dislocations gather and merge to form voids in grain boundaries in alloy. The voids grow and join, resulting in intergranular fracture. If voids occur at higher temperature, they could exist in grain boundaries and grain inside, which tend to occur void fracture. Because DO<sub>3</sub>-ordered Fe<sub>3</sub>Al without V has low cleavage strength and its super dislocations cross slip very difficult, the generation and growth of void could be retarded or limited during tension<sup>[10]</sup>. As degree of ordering in DO<sub>3</sub> Fe<sub>3</sub>Al without V decreases reduced rapidly above 350 °C, the deformation was controlled by the mechanism which changed gradually from super dislocations to ordinary unit dislocations. It led to increase in cross slip of dislocations and then generation and growth of voids. The fracture mode becomes void type in that condition. Addition of V increased the fracture strength of Fe<sub>3</sub>Al and produced some intergranular fracture, which suggested that V increased cleavage strength of Fe<sub>3</sub>Al, resulting in larger plastic deformation before fracture, so Fe<sub>3</sub>Al containing V



**Fig. 2** Fracture surfaces of Fe 28Al alloy at 25  $^{\circ}$ C (a) and at 500  $^{\circ}$ C (b), Fe 28Al 1.5 V alloy at 25  $^{\circ}$ C (c) and at 500  $^{\circ}$ C (d)

had better ductility at room temperature. Besides, V increases  $DO_3$ -existing temperature and retained  $DO_3$ -ordered structure at higher temperature may retard void fracture to take place at higher temperatures than  $Fe_3Al$  without V.

## 3 CONCLUSIONS

- 1) V refines grains and changes DO<sub>3</sub>-ordered Fe<sub>3</sub>Al fracture mode from transgranular cleavage to transgranular cleavage intergranular mixed type.
- 2) V raises the temperature related to DO<sub>3</sub>-ordered Fe<sub>3</sub>Al strength peak about 200 °C, which can make DO<sub>3</sub> Fe<sub>3</sub>Al alloy to be applied above 600 °C.

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