

Catalytic graphitization of polyacrylonitrile (PAN)-based carbon fibers with Fe-Cr₂O₃ composite coating

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Received 28 July 2009; accepted 30 October 2009

Abstract: The process of electrodepositing Fe-Cr₂O₃ composite coating on polyacrylonitrile (PAN)-based carbon fibers and its catalytic graphitization were studied. Carbon fibers with and without electrodeposited Fe-Cr₂O₃ composite coating were heat treated at different temperatures and the structural changes were characterized by XRD, Raman spectroscopy and SEM. The results indicate that Fe-Cr₂O₃ composite coating exhibits a significant catalytic effect on graphitization of carbon fibers at low temperatures. When the Fe-Cr₂O₃-coated carbon fibers were heat treated at 1 300 °C, the interlayer spacing (d_{002}) and ratio of relative peak area (A_D/A_G) reach 3.364 Å and 0.34, respectively. Whereas, the extent of graphitization of pristine carbon fibers is comparatively low even after heat treatment at 2 800 °C and the values of d_{002} and A_D/A_G are 3.414 Å and 0.68, respectively. The extent of graphitization of carbon fibers increases not only with the increase of the catalyst gross but also the Cr₂O₃ content in Fe-Cr₂O₃ coating. The catalytic effect of Fe-Cr₂O₃ composite coating accords with the dissolution–precipitation mechanism.

Key words: carbon fiber; catalytic graphitization; Fe-Cr₂O₃ coating

1 Introduction

It is well known that graphite has many unique properties, such as high electric conductivity, high thermal conductivity and high resistance to strong acid and alkali. These unique properties result in many potential applications, such as catalyst support[1–2], sensor[3–4], Li-ion battery[5] and electrochemical capacitor[6]. However, the properties of graphitic materials such as thermal and electric conductivities, and tensile modulus can be affected by the extent of graphitization. Therefore, extent of graphitization is an important parameter for the application of carbon materials. Usually, the heat treatment temperature (HTT) of carbon was above 3 000 °C. Adding catalysts could accelerate the graphitization of carbon[7–8], which is called catalytic graphitization. In previous works, transition metals have been used as catalyst precursors for graphitization. WEISWEILER et al[9] studied the graphitization of monolithic glasslike carbon with metals as catalysts, and they concluded that elements such as Co, Fe, Pt, Mo, Cr and B were highly effective in catalyzing

the graphitization. Lately, MALDONADO-HODAR et al[10] used various kinds of metals to produce graphite and considered that Cr and Fe seemed to be the best catalysts for graphitization of carbon aerogels. Metallic coating was easily electrodeposited on the surface of PAN-based carbon fibers, and the electrodeposited metallic coating has an obvious catalytic effect on the graphitization of the carbon fiber after high temperature treatment[11]. In order to obtain carbon fibers with high extent of graphitization at low temperatures, in this work, the catalytic graphitization of carbon fibers with electrodeposited Fe-Cr₂O₃ composite coating was studied. Moreover, effects of the Cr₂O₃ content in Fe-Cr₂O₃ composite coating and the deposition time of the coating on the extent of graphitization of carbon fibers were investigated.

2 Experimental

2.1 Preparation of samples

Carbon fibers used in this study were PAN-based carbon fibers (T700-12K) produced by Toray Corporation in Japan. Fe-Cr₂O₃ composite coatings were

electrodeposited on carbon fibers using ferrous sulfate and chromic oxide as the source of iron and chromium, respectively, boric acid as buffer, sodium chloride as conductive salt and sulfamic acid as complex agent. Before electrodeposition, the carbon fibers need some appropriate pretreatments. At first, the sizing material of carbon fibers was removed by immersing carbon fibers into acetone solution for 30 min. And then the carbon fibers were rinsed by double distilled water. Afterwards, alkaline liquid (NaOH 80 g/L, Na₃PO₄ 30 g/L and Na₂CO₃ 15 g/L) was used to treat carbon fibers for 15 min at 60 °C. Ultrasonic vibration was applied during this process and finally the carbon fibers were rinsed by double distilled water for 5 min. The content of Cr₂O₃ in the Fe-Cr₂O₃ composite coatings was altered by changing the concentration of Cr₂O₃ in electrolyte. Tables 1 and 2 list the bath composition and deposition parameters, respectively. Heat treatment of the bare carbon fibers and Fe-Cr₂O₃-coated carbon fibers was carried out in a graphite furnace under an argon atmosphere. Temperature was increased at the rate of 40 °C/min and kept for 120 min until it reached the targeted temperature.

Table 1 Bath composition used for electrodepositing Fe-Cr₂O₃ composite coating (g/L)

Ferrous sulfate (FeSO ₄ ·7H ₂ O)	Chromic oxide (Cr ₂ O ₃)	Boric acid (H ₃ BO ₃)	Sodium chloride (NaCl)	Sulfamic acid (NH ₂ SO ₃ H)
350	0–65	35	80	25

Table 2 Deposition conditions used for electrodepositing Fe-Cr₂O₃ composite coating

Bath temperature/°C	Current density/ (A·dm ⁻²)	Deposition time/min	Solution pH	Stirring speed/ (r·s ⁻¹)
50	3	0–25	2	50

2.2 Characterization

The degree of graphitization of the fiber was investigated by powdered sample X-ray diffractometry (Cu K_α radiation, 40 kV, 200 mA). Silicon was used as a internal standard. The values of the interlayer spacing d_{002} and crystalline size L_c were calculated from the (002) diffraction peak according to the method described by Bragg law and Scherrer equation[12]. The degree of graphitization can be calculated by the following equation: $G = (3.440 - d_{002}) / (3.440 - 3.354)$ [12–13], where G refers to the degree of graphitization (%), 3.440 represents the interlayer spacing of the fully non-graphitized carbon (Å), 3.354 represents the interlayer spacing of the ideal graphite crystallite and d_{002} refers to the interlayer spacing derived from XRD pattern(Å).

The structural changes of the PAN-based carbon fibers after high temperature heat treatment were observed by a JEOL JSM-5600LV scanning electron microscope (SEM) at an accelerating voltage of 15 kV. The extent of graphitization at different locations of the cross-section of the heat treated carbon fibers was obtained with a LABRAM-010 Raman microscopy (632.83 nm He-Ne laser, laser beam diameter 3 μm) in the range of 1 100–1 880 cm⁻¹.

In addition, the element distribution inside the Fe-Cr₂O₃-coated fiber after heat treatment was characterized by an energy dispersive analysis system of X-ray (EDS) attached to the JSM-5600LV SEM.

3 Results and discussion

3.1 Effect of heat treatment temperature

Fig.1 indicates the SEM images of bare carbon fiber and carbon fiber coated with Fe-Cr₂O₃. As shown in Fig.1(b), Fe-Cr₂O₃ composite coating can be observed on the carbon fiber substrate after electrochemical deposition. The surface of the Fe-Cr₂O₃ composite coating is very rough and the Cr₂O₃ particulates disperse in the coating. Fig.2 shows the XRD pattern and Raman spectra of carbon fibers without coating at different heat treatment temperatures (HTTs). In Fig.2(a), the (002)

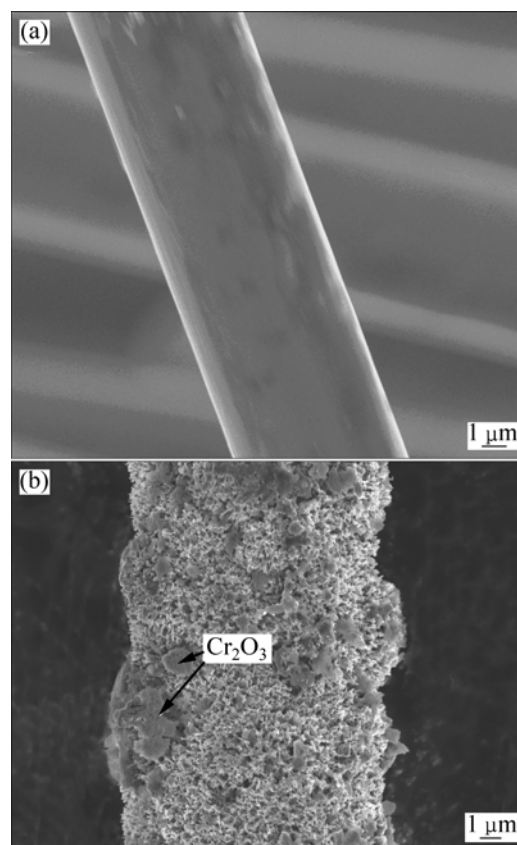


Fig.1 SEM images of bare carbon fiber (a) and carbon fiber coated with Fe-Cr₂O₃ composite coating (b)

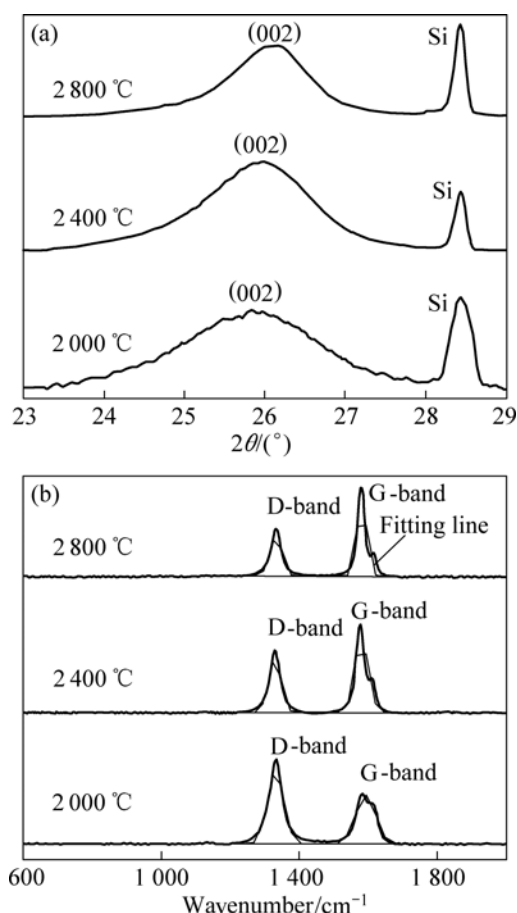


Fig.2 XRD patterns (a) and Raman spectra (b) of PAN-based carbon fibers heat treated at different temperature

peak shifts right distinctly when the HTT increases. Moreover, the broad profile gets sharper increasingly. Fig.2(b) exhibits two relatively broad Raman bands at about $1\,350\text{ cm}^{-1}$ (D-band) and $1\,580\text{ cm}^{-1}$ (G-band), which are responsible for the disordered carbon atoms and the graphitic phase, respectively[14–15]. As shown in Fig.2(b), the shapes of D and G bands become sharper and D-band is gradually weakened with increasing HTT. However, G-band is distinctly strengthened, because graphite component increases and disordered carbon decreases contrarily.

Table 3 lists the values of d_{002} , the thickness of crystallized carbon layers (L_c) and Raman spectroscopic parameters of carbon fibers after heat treatment at different HTTs. The closer the value of d_{002} is to 3.354 Å and the larger the value of L_c is, the higher the extent of graphitization is. Moreover, a smaller value of the relative peak area (A_D/A_G) also means a higher extent of graphitization[15–16]. It can be seen from Table 3 that the ratio of A_D/A_G and the wavenumber of D and G bands all decrease with increasing HTT. From Fig.2 and Table 3, it is noted that the extent of graphitization increases with the increase of HTT. However, PAN-based carbon fibers without Fe- Cr_2O_3 composite coating are hard to be

Table 3 Effects of HTT on d_{002} , L_c and Raman spectroscopic parameters of PAN-based carbon fibers

Sample number	HTT/°C	$d_{002}/\text{Å}$	$L_c/\text{Å}$	Wavenumber/ cm^{-1}		A_D/A_G
				D-band	G-band	
1	2 000	3.443	49	46	57	1.25
2	2 400	3.434	57	37	41	0.71
3	2 800	3.414	74	35	28	0.68

graphitized even being heat treated at $2\,000\text{ °C}$. When the HTT is raised to $2\,800\text{ °C}$, the value of L_c is just 74 Å and the value of d_{002} reaches 3.414 Å , for instance. The XRD patterns and Raman spectra of PAN-based carbon fibers coated with Fe- Cr_2O_3 ($\text{Cr}_2\text{O}_3\text{ }20\text{ g/L}$, 15 min) through heat treatment at different temperatures are shown in Fig.3. The (002) peak shifts right and becomes sharper as the HTT increases (Fig.3(a)). Raman spectroscopic parameters (wavenumber and the ratio of peak area) are obtained after curve fitting, as shown in Fig.3(b). Table 4 lists the values of d_{002} , L_c and Raman spectroscopic parameters, and shows that the value of L_c increases with the increase of HTT, but the value of d_{002} decreases with the increase of HTT. When the HTT is raised to $1\,300\text{ °C}$, the value of L_c is 271 Å and the value of d_{002} reaches 3.364 Å that is very close to 3.354 Å

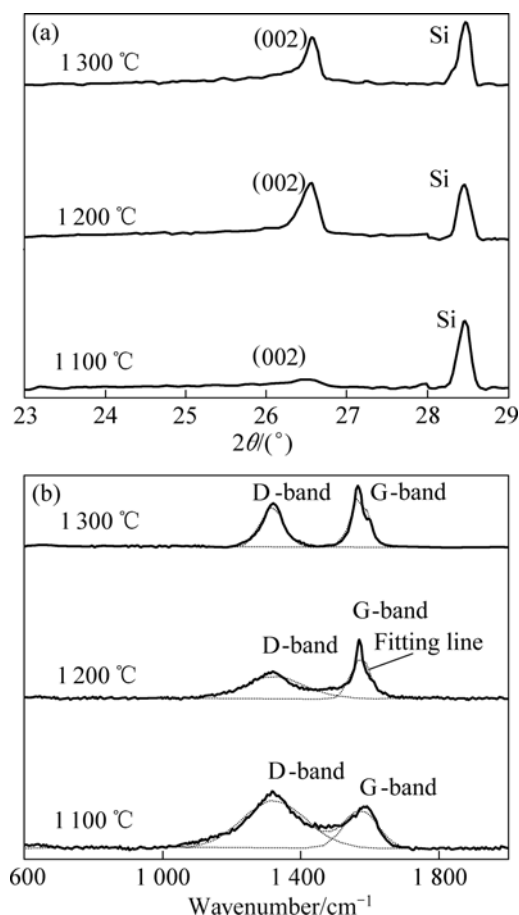


Fig.3 XRD patterns (a) and Raman spectra (b) of PAN-based carbon fibers coated with Fe- Cr_2O_3 composite coating

for hexagonal graphite. From Table 4, it can be found that the wavenumber and the ratio of peak area (A_D/A_G) in Raman spectra decrease with the increase of HTT. It is also noted that the G-band wavenumber for Fe-Cr₂O₃ coated carbon fibers heat treated at 1 300 °C is 22 cm⁻¹, which is close to the value of highly oriented graphite (21 cm⁻¹)[16]. Although the HTTs of Fe-Cr₂O₃ coated carbon fibers are lower than those of bare carbon fibers, Fe-Cr₂O₃ coated carbon fibers have higher extent of graphitization than bare carbon fibers, which shows that Fe-Cr₂O₃ coating has catalytic effect on graphitization of PAN-based carbon fibers.

Table 4 Effects of HTT on d_{002} , L_c and Raman spectroscopic parameters of PAN-based carbon fibers coated with Fe-Cr₂O₃ composite coating

Sample number	HTT/°C	$d_{002}/\text{Å}$	$L_c/\text{Å}$	Wavenumber /cm ⁻¹		A_D/A_G
				D-band	G-band	
1	1 100	3.400	66	184	95	2.43
2	1 200	3.369	194	182	54	1.74
3	1 300	3.364	271	84	22	0.34

3.2 Catalytic effect of Cr₂O₃ content in Fe-Cr₂O₃ composite coating

The Cr₂O₃ content in the Fe-Cr₂O₃ composite coating was altered by changing the concentration of Cr₂O₃ in electrolyte. Table 5 lists the effects of Cr₂O₃ concentration on the values of d_{002} , L_c and Raman spectroscopic parameters of Fe-Cr₂O₃ coated carbon fibers (electrodeposited for 15 min) heat treated at 1 200 °C. It is noted that d_{002} and A_D/A_G decrease with the increase of Cr₂O₃ concentration. A low L_c of 141 Å is obtained for carbon fibers coated with pure Fe. However, with the increase of Cr₂O₃ concentration in the electrolyte, there is an evident increase in L_c . Simultaneously, the wavenumbers of peaks decrease. As the Cr₂O₃ concentration rises to 50 g/L, L_c reaches 288 Å, d_{002} and A_D/A_G reach 3.357 Å and 0.60, respectively. The XRD and Raman spectra results show that much better graphitization can be achieved for carbon fibers with higher Cr₂O₃ content. In general, the catalyst content has a significant effect on graphitization at the same HTT[17–18]. Table 6 lists the changes of XRD data (d_{002} and L_c) and Raman spectroscopic parameters of carbon fibers with different Fe-Cr₂O₃ deposition time (Cr₂O₃ 20 g/L) at HTT of 1 200 °C. It is clear that the catalytic graphitization effect of PAN-based carbon fibers increases with the increase of Fe-Cr₂O₃ deposition time, i.e. Fe-Cr₂O₃ content. Therefore, the extent of graphitization is related not only to Cr₂O₃ content but also to catalyst gross. As the deposition time increases from 5 min to 25 min, a decrease in A_D/A_G value, from

2.28 to 1.24, was found. However, a significant decrease of A_D/A_G from 1.79 to 0.60 was obtained, when the Cr₂O₃ concentration increases from 10 g/L to 50 g/L. Above experimental results show that Cr₂O₃ content has a much more prominent catalytic effect on the graphitization of carbon fibers.

Table 5 Effects of Cr₂O₃ concentration on d_{002} , L_c and Raman spectroscopic parameters of Fe-Cr₂O₃-coated PAN-based carbon fibers heat treated at 1 200 °C

Sample number	$\rho(\text{Cr}_2\text{O}_3)/(\text{g}\cdot\text{L}^{-1})$	$d_{002}/\text{Å}$	$L_c/\text{Å}$	Wavenumber /cm ⁻¹		A_D/A_G
				D-band	G-band	
1	0	3.373	141	194	86	2.35
2	10	3.369	196	193	80	1.79
3	20	3.369	194	182	54	1.74
4	30	3.362	203	146	42	1.66
5	50	3.357	288	89	27	0.60

Table 6 Effects of deposition time on d_{002} , L_c and Raman spectroscopic parameters of Fe-Cr₂O₃-coated PAN-based carbon fibers heat treated at 1 200 °C

Sample number	Deposition time/min	$d_{002}/\text{Å}$	$L_c/\text{Å}$	Wavenumber /cm ⁻¹		A_D/A_G
				D-band	G-band	
1	5	3.400	67	198	101	2.28
2	15	3.369	194	182	54	1.74
3	25	3.361	204	81	34	1.24

3.3 Catalytic mechanism for graphitization

Fig.4(a) and Fig.4(b) show the SEM images of the cross-section of original carbon fiber and carbon fiber coated with catalyst after heat treatment at 1 200 °C, respectively. The cross-section of the original carbon fiber has a flat surface. While being heat treated at 1 200 °C, the cross-section of fiber changes from a flat surface to a rough surface after catalytic graphitization. It is also observed that the outside of the carbon fiber is rougher than the center and the untransformed portion of the carbon fiber with a typical flat can be found in the centre (Fig.4(b)), indicating that the catalytic graphitization process is incomplete. It is speculated that Fe and Cr₂O₃ in the composite coating are responsible for the catalytic graphitization. In order to verify the effect of Fe and Cr₂O₃, the distribution location of Fe and Cr₂O₃ on cross-section of fiber is detected by energy dispersive spectrometry (EDS). A linear scanning was carried out along the arrow in Fig.4(b). The EDS results in Fig.4(c) show that Fe and Cr mainly remain in the rough layer, which implies that most of the coatings move towards the center of cross-section but Fe and Cr do not arrive at the center. The reason for these results is that the process of catalytic graphitization proceeds from the outer

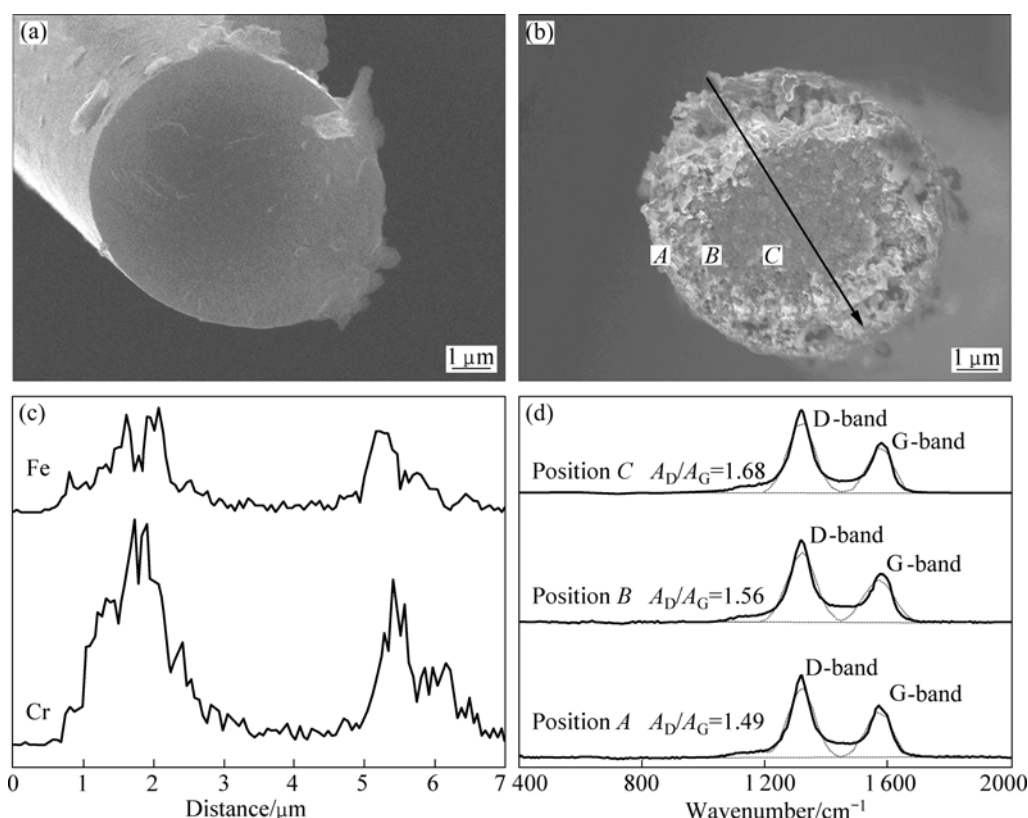


Fig.4 SEM images of cross-section of original carbon fiber (a), carbon fiber coated with Fe-Cr₂O₃ (b), corresponding EDS (c) and corresponding Raman spectra (d)

surface where the fiber contacts the catalyst[19]. Fe and Cr are ejected from the original composite coating and move towards the carbon region and a graphitic phase precipitates behind the catalyst following the well-known dissolution–precipitation mechanism. According to the mechanism, the extent of graphitization should become higher increasingly from the centre to the outer surface. Raman analysis was carried out on the, positions *A*, *B* and *C*, respectively, in Fig.4(b). The Raman spectra results are shown in Fig.4(d). The A_D/A_G values of 1.49, 1.56 and 1.68 corresponding to positions *A*, *B* and *C*, respectively, indicate that the outer portion has a higher extent of graphitization. Apparently, the phenomena are also consistent with the dissolution–precipitation mechanism.

4 Conclusions

1) The Fe-Cr₂O₃ composite coating was electrodeposited on the surface of PAN-based carbon fibers by galvanostatic deposition method. Much better graphitization can be achieved for carbon fibers at lower heat treatment temperature when the Fe-Cr₂O₃ catalyst is present. The Fe-Cr₂O₃-coated carbon fiber treated at 1 300 °C has a higher extent of graphitization than the bare carbon fiber treated at 2 800 °C, and their d_{002}

values are 3.364 and 3.414 Å, respectively.

2) Not only the Cr₂O₃ content but also the catalyst gross (deposition time) has an important effect on the catalytic graphitization of the Fe-Cr₂O₃-coated carbon fiber. The extent of graphitization of the Fe-Cr₂O₃ coated carbon fibers increases with the increase of Fe-Cr₂O₃ deposition time at the same HTT. Moreover, the extent of graphitization of the Fe-Cr₂O₃-coated carbon fibers increases with the increase of Cr₂O₃ content in the Fe-Cr₂O₃ composite coating at the same HTT. As the Cr₂O₃ concentration in electrolyte rises from 0 to 50 g/L, the value of A_D/A_G decreases from 2.35 to 0.60, and the L_c rises from 141 to 288 Å.

3) The catalytic graphitization of Fe-Cr₂O₃ coating follows the dissolution–precipitation mechanism. The catalytic graphitization phenomenon first occurs along the outside of the fiber and the extent of graphitization becomes high increasingly from the centre to the outer surface.

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(Edited by LI Xiang-qun)