

## Synthesis of $\text{Ti}_3\text{SiC}_2$ by spark plasma sintering (SPS) of elemental powders<sup>①</sup>

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**Abstract:**  $\text{Ti}_3\text{SiC}_2$  materials have been fabricated by spark plasma sintering of the elemental powders with the addition of Al. At the heating rate of 80 °C/min and under the pressure of 30 MPa, the ideal synthesis temperature of  $\text{Ti}_3\text{SiC}_2$  is in the range of 1 150 ~ 1 250 °C. The addition of Al is in favor of the formation of  $\text{Ti}_3\text{SiC}_2$ . The synthesized compound has the molecular of  $\text{Ti}_3\text{Si}_{0.8}\text{Al}_{0.2}\text{C}_2$  and lattice parameters of  $a = 0.3069 \text{ nm}$ ,  $c = 1.7670 \text{ nm}$ . Its grain is plane shape with a size of about 50  $\mu\text{m}$  in the elongated dimension. The prepared material has Vickers hardness of 3.5 ~ 5.5 GPa (at 1 N and 15 s) and is as readily machinable as graphite's.

**Key words:**  $\text{Ti}_3\text{SiC}_2$ ; synthesis; spark plasma sintering

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### 1 INTRODUCTION

Recently, titanium silicon carbide ( $\text{Ti}_3\text{SiC}_2$ ) has received considerable attention because of the unusual combination of good properties that makes it a candidate for many high temperature applications<sup>[1]</sup>. It has excellent machinability, and it is not sensitive to thermal shock. At room temperature, it has electrical and thermal conductivities of  $4.5 \times 10^6 \text{ s} \cdot \text{m}^{-1}$  and  $37 \text{ W}/(\text{m} \cdot \text{K})$ , respectively<sup>[1, 3]</sup>.  $\text{Ti}_3\text{SiC}_2$  has a Vickers hardness of 4 GPa, elastic modulus of 325 GPa and a room temperature fracture toughness of  $7 \text{ MPa} \cdot \text{m}^{1/2}$ <sup>[2]</sup>. Its coefficient of thermal expansion is  $9.2 \times 10^{-6} \text{ K}^{-1}$ <sup>[1, 3]</sup>.  $\text{Ti}_3\text{SiC}_2$  is also a damage-tolerant material and has a brittle-to-plastic transition at 1 200 °C. At 1 300 °C, the material is plastic with 'yield' points of 100 and 500 MPa in flexure and compression, respectively<sup>[4]</sup>. When samples with large oriented grains (2 ~ 4 mm) are tested under compression, the material exhibits macro-plasticity at room temperature by forming shear and kink bands<sup>[5]</sup>. It shows parabolic oxidation behavior in air in the temperature range of 900 ~ 1 400 °C with an activation energy of  $370 \pm 20 \text{ J/mol}$ <sup>[6]</sup>. Additionally,  $\text{Ti}_3\text{SiC}_2$  is an exceptional solid lubricant with an ultra-friction of  $(2 \sim 5) \times 10^{-3}$ <sup>[7]</sup>.

While there is general agreement regarding the attractive attributes of  $\text{Ti}_3\text{SiC}_2$ , its synthesis with both high purity and density is difficult. Although the ternary has

been synthesized by CVD<sup>[8, 9]</sup>, the gaseous reaction method is limited in a small-scale production. Many solid-state synthesis methods via different starting powders have been investigated in order to fabricate bulk monolithic  $\text{Ti}_3\text{SiC}_2$ . However, the solid-state synthesized  $\text{Ti}_3\text{SiC}_2$  usually contains a small amount of TiC and/or SiC as impurities. Recently, Ranghy and Barsoum<sup>[10]</sup> successfully fabricated high-purity  $\text{Ti}_3\text{SiC}_2$  polycrystals by reactively hot-pressing the mixture of Ti, graphite and SiC powders, but the fabricating process was very complex. Thus further work is needed to develop new methods for the synthesis of  $\text{Ti}_3\text{SiC}_2$ . In the present research, synthesis of  $\text{Ti}_3\text{SiC}_2$  by spark plasma sintering of the elemental powders is reported. And because  $\text{Ti}_3\text{AlC}_2$  has the same structure and similar properties as those of  $\text{Ti}_3\text{SiC}_2$ <sup>[11]</sup>, the effect of Al on the formation of  $\text{Ti}_3\text{SiC}_2$  is especially investigated.

### 2 EXPERIMENTAL

Commercially available Ti, Si, Al and graphite powders were used as raw materials to synthesize  $\text{Ti}_3\text{SiC}_2$  by spark plasma sintering. The characteristics of starting powders are listed in Table 1. The mixture with a designed composition was firstly mixed in ethanol for 24 h and then was filled into graphite crucibles with 20 mm in diameter and finally sintered in Spark Plasma Sintering System (Dr SINTER1020, Izumi Technology Co. Ltd.).

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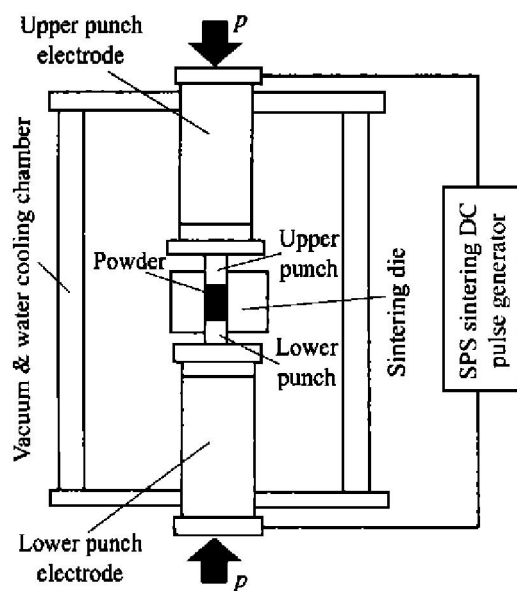
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Fig. 1 shows the schematic diagram of the system. The samples were heated at a rate of  $80\text{ }^\circ\text{C}/\text{min}$ , in vacuum of  $0.5\text{ Pa}$ , and under the pressure of  $30\text{ MPa}$  in the preparing process. When the temperatures reached the designed sintering one, soak the sample at that temperature for 10 min. The sintering temperature ranges from  $1\text{ }100\text{ }^\circ\text{C}$  to  $1\text{ }300\text{ }^\circ\text{C}$ .

**Table 1** Characteristics of starting powders

Starting powder	Content/ %	Average size/ $\mu\text{m}$
Ti	99.0	35
Si	99.5	28
Al	99.8	40
C	99.0	2



**Fig. 1** Schematic of spark plasma sintering system

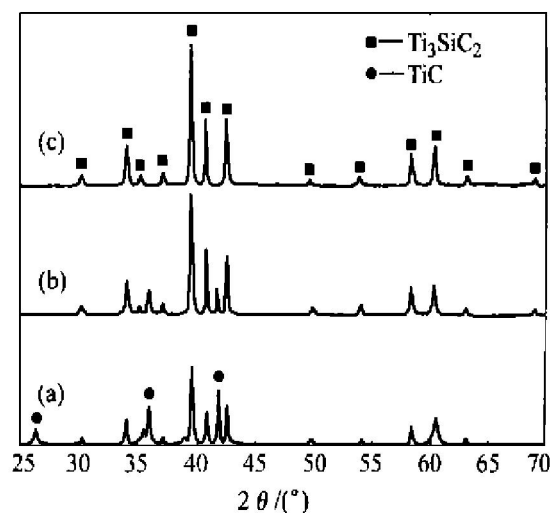
The sintered product was characterized by XRD method to determine the phases and lattice parameters. The lattice parameters were calculated by Rietveld analysis and measured with Si as a standard additive. The density of the sintered product was measured by Archimedes' method and compared with the theoretical density derived from the lattice constants. The measurement of its Vickers hardness was carried out at  $1\text{ N}$  for  $15\text{ s}$  by using a large polarizing microscope. Their chemical analyses of minerals were performed in a JEOL JCXA-733 electron probe microanalysis (EPMA) with three wavelength-dispersive spectrometers. A scanning electronic microscope (SEM) was used to investigate the microstructure of the material.

### 3 RESULTS AND DISCUSSION

#### 3.1 Effect of addition of Al on synthesis of $\text{Ti}_3\text{SiC}_2$

It has been reported that the purity of  $\text{Ti}_3\text{SiC}_2$  synthesized from Ti/Si/C powders was very sensitive to the discrepancy from its stoichiometric composition. The defi-

ciency of Si usually favors the formation of  $\text{TiC}$ <sup>[12, 13]</sup>. The loss of Si might occur by evaporation as the sample fired in Ar or vacuum, resulting in product containing quite a large amount of  $\text{TiC}$ . Li<sup>[13]</sup> synthesized high pure  $\text{Ti}_3\text{SiC}_2$  material by using a starting composition with 20% Si more than that suggested by stoichiometry of  $\text{Ti}_3\text{SiC}_2$ . In the present research, samples with three different starting composition in molar fraction ratio (a)  $x(\text{Ti}):x(\text{Si}):x(\text{C}) = 3:1:2$ ; (b)  $x(\text{Ti}):x(\text{Si}):x(\text{C}) = 3:1.2:2$ ; (c)  $x(\text{Ti}):x(\text{Si}):x(\text{Al}):x(\text{C}) = 3:1:0.2:2$ , were investigated. The powder mixtures were sintered in the spark plasma sintering system at  $1\text{ }250\text{ }^\circ\text{C}$  for 10 min. Fig. 2 shows the X-ray diffraction patterns of resultant products. The main phase of the samples was  $\text{Ti}_3\text{SiC}_2$ . No second phase was identified by X-ray diffraction in sample (c), but both sample(a) and sample(b) contained quite a large amount of  $\text{TiC}$  and the content of  $\text{TiC}$  in sample(a) was much higher than that in sample(b). The results confirmed our initial expectation that the addition of Al would be in favor of the synthesis of  $\text{Ti}_3\text{SiC}_2$ . Therefore, the composition of sample(c) was chosen as that of the samples used in the following experiments.



**Fig. 2** X-ray diffraction patterns of resultant products sintered at  $1250\text{ }^\circ\text{C}$  from different starting compositions

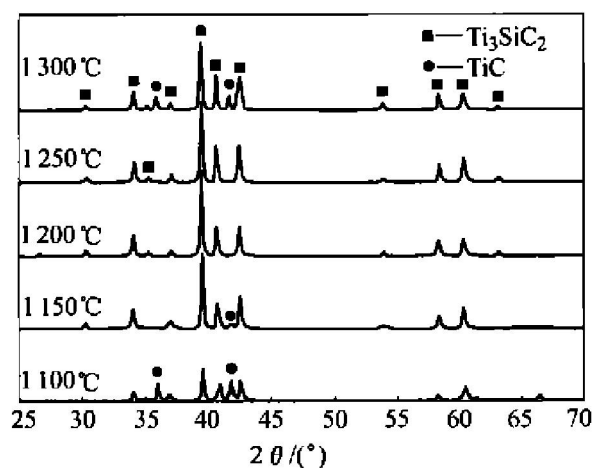
- (a)  $-x(\text{Ti}):x(\text{Si}):x(\text{C}) = 3:1:2$ ;  
 (b)  $-x(\text{Ti}):x(\text{Si}):x(\text{C}) = 3:1.2:2$ ;  
 (c)  $-x(\text{Ti}):x(\text{Si}):x(\text{Al}):x(\text{C}) = 3:1:0.2:2$

#### 3.2 Influence of sintering temperature

Fig. 3 shows the X-ray diffraction patterns of the resultant products sintered at different temperatures. When sintered at  $1\text{ }100\text{ }^\circ\text{C}$ , the product mainly consisted of  $\text{Ti}_3\text{SiC}_2$  and  $\text{TiC}$ , which suggested that  $\text{Ti}_3\text{SiC}_2$  formed in large quantity at that temperature, but there was still a great amount of  $\text{TiC}$ . When a sample was sintered at  $1\text{ }150\text{ }^\circ\text{C}$ , the formation of  $\text{Ti}_3\text{SiC}_2$  almost completely finished and only a very weak peak of  $\text{TiC}$  ( $2\theta = 41.82^\circ$ )

was identified by X-ray diffraction. When sintering temperature reached at 1 200 °C or 1 250 °C, no phase but  $\text{Ti}_3\text{SiC}_2$  was identified by X-ray diffraction, which indicated that the products were pure  $\text{Ti}_3\text{SiC}_2$ . But at 1 300 °C, TiC appeared again, and the X-ray diffraction peaks of  $\text{Ti}_3\text{SiC}_2$  became weaken at the same time. That the appearance of TiC at 1 300 °C is due to either the decomposition of  $\text{Ti}_3\text{SiC}_2$ , or the rapid loss of Si causing the decrease of the content of  $\text{Ti}_3\text{SiC}_2$  by evaporation in large quantities at high heating rate, is still unclear.

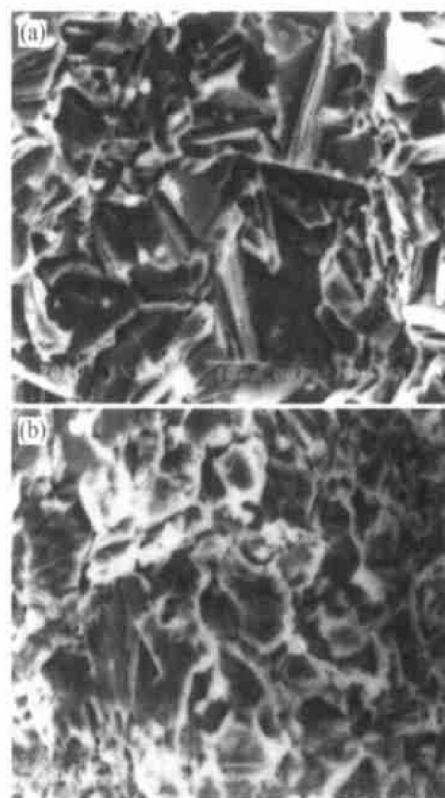
The measured lattice parameters of  $\text{Ti}_3\text{SiC}_2$  solid solution were  $a = 0.3069 \text{ nm}$ ,  $c = 1.7670 \text{ nm}$ , respectively, being very close to those reported by other authors<sup>[6, 7]</sup>. It was clear that the solid solution of Al in  $\text{Ti}_3\text{SiC}_2$  barely changed the lattice parameters. The measured densities of bulk materials sintered at 1 200 °C and 1 300 °C were 4.40 and 4.43  $\text{g/cm}^3$ , that were 97.2% and 97.9% of theoretic density of  $\text{Ti}_3\text{SiC}_2$ , respectively. It can be concluded that high pure  $\text{Ti}_3\text{SiC}_2$  material can be synthesized by SPS from the starting powders mixtures with a molar fraction ratio  $x(\text{Ti}) : x(\text{Si}) : x(\text{Al}) : x(\text{C}) = 3 : 1 : 0.2 : 2$ .



**Fig. 3** X-ray diffraction patterns of resultant products sintered at different temperatures

### 3.3 Composition and microstructure

The sample synthesized at 1 200 °C was examined by EPMA. Its composition analysis was performed at 15 different positions. The results showed that  $x(\text{Si}) : x(\text{Al})$  (mole fraction, %) in the sample ranged from 75.6:24.4 to 87.2:12.8 and the average result is 80.8:19.2, which indicated the synthesized mineral has the molecular of  $\text{Ti}_3\text{Si}_{0.8}\text{Al}_{0.2}\text{C}_2$ . Fig. 4 showed the SEM fractograph of samples sintered at 1 200 °C and 1 250 °C, respectively, which revealed the materials consist of densely packed plane-shape grains and the maximum size in the plane of these grains is about 50  $\mu\text{m}$  and the processing temperature affected the plane-shape grain size of  $\text{Ti}_3\text{SiC}_2$ .



**Fig. 4** SEM fractographs of  $\text{Ti}_3\text{SiC}_2$  material synthesized by SPS  
(a) —1 200 °C; (b) —1 250 °C

### 3.4 Vickers hardness and machinability

The measured Vickers hardness of the products sintered at the temperatures of 1 200 °C and 1 250 °C was in the range of 3.5 ~ 5.5 GPa, which is slightly smaller than other reported results. It is perhaps the solid solution of Al in  $\text{Ti}_3\text{SiC}_2$  reduced its hardness. More importantly, the material has the same machinability as graphite's. It could easily be machined with ordinary machining tools, and holes could readily be drilled by using common steel drills without lubrication.

## 4 CONCLUSIONS

1) The addition of Al is in favor of the synthesis of  $\text{Ti}_3\text{SiC}_2$ . Pure  $\text{Ti}_3\text{SiC}_2$  solid solution is synthesized by spark plasma sintering an elemental powder mixture with a composition of  $x(\text{Ti}) : x(\text{Si}) : x(\text{Al}) : x(\text{C}) = 3 : 1 : 0.2 : 2$  in molar fraction ratio. The ideal synthesis temperature ranged from 1 150 °C to 1 250 °C, which is the lowest temperature for fabricating pure  $\text{Ti}_3\text{SiC}_2$  material so far.

2) The lattice parameters of  $\text{Ti}_3\text{SiC}_2$  solid solution are  $a = 0.3066 \text{ nm}$ ,  $c = 1.7670 \text{ nm}$ , respectively. The synthesized mineral has the molecular of  $\text{Ti}_3\text{Si}_{0.8}\text{Al}_{0.2}\text{C}_2$ . The grain is plane-shape with a maximum size in the plane of about 50  $\mu\text{m}$ .

3) The obtained material has Vickers hardness of 3.

5 – 5.5 GPa and could be easily machined by using ordinary machining tools.

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