



## Facile microwave-assisted fabrication of WC–Al<sub>2</sub>O<sub>3</sub> composite powder from WO<sub>3</sub>–Al–C mixture

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**Abstract:** A facile and cheap method for the fabrication of WC–Al<sub>2</sub>O<sub>3</sub> composite powder was proposed. Thermodynamic calculations indicate that aluminothermic reduction of WO<sub>3</sub> in WO<sub>3</sub>:xAl:(4–1.5x)C mixture is accompanied by a great deal of heat, so carbothermic reduction reaction (endothermic) becomes activated in the system. By substitution of aluminum with carbon, the formation of unwanted W<sub>2</sub>C phase can be prevented because of less thermodynamic stability at lower temperatures. For the verification of the proposed reaction mechanism, various WO<sub>3</sub>:xAl:(4–1.5x)C mixtures (1.1 ≤ x ≤ 2) were heat-treated in a domestic microwave oven. The results showed that the type of reaction is self-propagating high temperature synthesis (SHS) when 1.4 ≤ x ≤ 2. Lower amount of Al in WO<sub>3</sub>:xAl:(4–1.5x)C mixtures results in a higher formation of WC. A W<sub>2</sub>C-free WC–Al<sub>2</sub>O<sub>3</sub> composite was obtained by continuation of microwave heating in an isolated atmosphere, after the occurrence of SHS reaction in a mixture containing 1.4 mol of Al. Results also showed that when x ≤ 1.3, type of reaction becomes gradual, which in turn brings about the incompleteness reaction and residue of initial reagents.

**Key words:** microwave heating; combustion synthesis; WC–Al<sub>2</sub>O<sub>3</sub> composite

### 1 Introduction

WC–Al<sub>2</sub>O<sub>3</sub> composites are useful materials for various industrial applications including production of drilling, cutting and machining tools as well as coating purposes. These composites show interesting properties such as low density, excellent hardness, good chemical inertness and high temperature strength [1–3].

Long time high temperature heating under a controlled atmosphere is the conventional method for the fabrication of WC/WC–Al<sub>2</sub>O<sub>3</sub> composites, which makes the products considerably expensive [4,5]. Hence, various synthesis methods have been evaluated in order to find a simple route which shortens the reaction time and utilizes cheap reagents [6–9]. One of these methods is self-propagating high temperature synthesis (SHS).

SHS method is only applicable to the exothermic reactions. During this process, the heat released by chemical reactions propagates through the mixture of reagents spontaneously and facilitates the process to go

forward [10,11]. According to Merzhanov's criterion, when adiabatic temperature (The highest that a system could reach under an adiabatic condition,  $T_{ad}$ ) of an exothermic system is higher than 1800 K, the synthesis reaction type would be SHS [12]. SHS reactions could be initiated by: 1) a furnace, 2) an electrical element attached to the surface of the sample and 3) an igniter mixture. This synthesis method has some advantages such as high synthesis rate, in-complexity, low process cost and ability to produce pure compounds [11,13,14].

ZHANG et al [7] and NIYOMWAS [8] have reported the SHS synthesis of WC–Al<sub>2</sub>O<sub>3</sub> powders by use of WO<sub>3</sub>–Al–C reagents. For this purpose, the SHS reaction was triggered by means of a tungsten wire. Their results showed that the product consists of unexpected W<sub>2</sub>C phase which has weak properties in comparison with WC. Several methods were used to decrease the amount of W<sub>2</sub>C compound in the product, such as use of mixture diluents (e.g., Al<sub>2</sub>O<sub>3</sub> and NaCl) [8] and/or employment of active carbon as the carbon source [7]. Moreover, it has been proved that W<sub>2</sub>C phase could be

leached from the product by use of a mixture of  $\text{HNO}_3$ – $\text{HF}$  acid [7].

Recently, activation of SHS reactions by microwave radiation has gained attention worldwide [15,16]. During microwave heating, interaction of electromagnetic wave and materials generates heat within the target. Thermal, magnetic and dielectric properties of the sample, as well as operating temperature, power and frequency of microwave influence the efficiency of heating process [17,18]. Since in microwave heating heat is generated within the materials, the temperature gradient is smaller than that of conventional heating routes; therefore, the product becomes more homogeneous [19]. Other benefits of use of microwave energy for heating are the decrease of production time and cost, ability of selective heating and less environmental pollution [20–22].

To the best of our knowledge, the first attempt on the microwave-assisted SHS synthesis of  $\text{WC}$ – $\text{Al}_2\text{O}_3$  composite powder is our work in Ref. [23]. It was found that the first reaction during microwave heating of  $\text{WO}_3$ – $\text{Al}$ – $\text{C}$  mixture is the aluminothermic reduction of  $\text{WO}_3$ . Tungsten carbide is subsequently obtained through the reaction of reduced tungsten and carbon. Our results showed that the product consists of  $\text{W}_2\text{C}$  phase whose formation is supposed to be related to: 1) occurrence of carbon deficiency in the system during synthesis process, and 2) high thermodynamic stability of this phase at high temperatures resulted from the great deal of heat released by the reaction between  $\text{WO}_3$  and  $\text{Al}$  [23]. According to the mentioned reaction mechanism, formation of  $\text{W}_2\text{C}$  phase could be prevented by A) adding extra amount of carbon to the initial  $\text{WO}_3$ – $\text{Al}$ – $\text{C}$  mixture and B) decreasing the system temperature to make  $\text{W}_2\text{C}$  phase thermodynamically unstable. Possibility of use of the first idea (idea A) for the production of  $\text{W}_2\text{C}$ -free product has been investigated in our previous study [23]. It was found that although the increase of carbon amount in the system diminishes  $\text{W}_2\text{C}$  phase, whole elimination of  $\text{W}_2\text{C}$  phase is unreachable due to some technical shortages of the employed experimental setup [23].

The aim of the present study is to investigate the feasibility of use of idea B for the fabrication of  $\text{WC}$ – $\text{Al}_2\text{O}_3$  composite powder from  $\text{WO}_3$ – $\text{Al}$ – $\text{C}$  mixture through microwave-assisted SHS process. This was achieved by substitution of some  $\text{Al}$  in reaction system with carbon. It is expected that lower  $\text{Al}$  content would decrease the maximum temperature obtained by aluminothermic reduction of  $\text{WO}_3$ , which in turn decreases the amount of  $\text{W}_2\text{C}$  phase in the product. For this purpose, various reagent mixtures were heated by means of a domestic microwave oven. Experimental observations together with the results obtained from

XRD and SEM examinations were used to find the optimum synthesis conditions. Thermodynamic calculations were used to predict the possibility of probable reactions in the systems.

## 2 Experimental

The aim of this study is to find a proper route for the prevention of  $\text{W}_2\text{C}$  phase formation during microwave heating of  $\text{WO}_3$ – $\text{Al}$ – $\text{C}$  mixture, through decreasing the maximum temperature of the system. Possibility of occurrence of probable reactions, type of reactions (endo/exothermic) and adiabatic temperature of reactions ( $T_{\text{ad}}$ ) were estimated by use of  $\Delta G_{298\text{ K}}^\circ$ ,  $\Delta H_{298\text{ K}}^\circ$  and  $T_{\text{ad}}$  values, respectively. Thermodynamic calculations were performed by use of LibreOffice Calc software [24] and required thermodynamic data were obtained from Factsage website [25].

Analytical grade  $\text{WO}_3$ ,  $\text{Al}$  and  $\text{C}$  powders were used as reagents. Various amounts of starting materials were mixed in a low energy laboratory ball-mill with hardened steel balls and pot. Milling was performed at room temperature in air atmosphere. Milling parameters were as follows: rotation speed 250 r/min, ball-to-powder mass ratio 10, time 5 min. Green cylindrical samples, with a constant volume (10 mm in diameter and 4 mm in height, mass ~2 g), were obtained by using a single-axis hydraulic press with a pressure of 50 MPa.

A SAMSUNG (GE2370G) domestic microwave oven with an output power of 850 W was used for microwave heating. Our prior examinations showed that the microwave absorption capability of the green samples is insufficient for a successful reaction ignition. Therefore, a silicon carbide ( $\text{SiC}$ ) block was placed under the samples to act as a susceptor and accelerate the heating [26,27]. Figure 1 illustrates a schematic of the experimental setup of this study.

Alumina blocks and powder as well as Pyrex beaker do not affect the heating process due to the high transparency of  $\text{SiO}_2$  and  $\text{Al}_2\text{O}_3$  compounds to microwave radiation [19,26]. These materials were merely used in the setup to create an air isolated atmosphere for the samples.

The occurrence of SHS reaction was identified by observing the physical phenomena, such as flushing and inflaming of the samples during the heating process. It was observed that SHS reactions occur within 1 min of microwave heating. For mixtures with a gradual reaction mode, heating for 2 min was allowed.

After heating for appropriate time, microwave device was turned off and samples were allowed to cool down naturally. Obtained powders were analyzed by use of an X-ray diffraction instrument (XRD: JEOL-JDX8030 with a  $\text{Cu K}_\alpha$  radiation). Microstructures

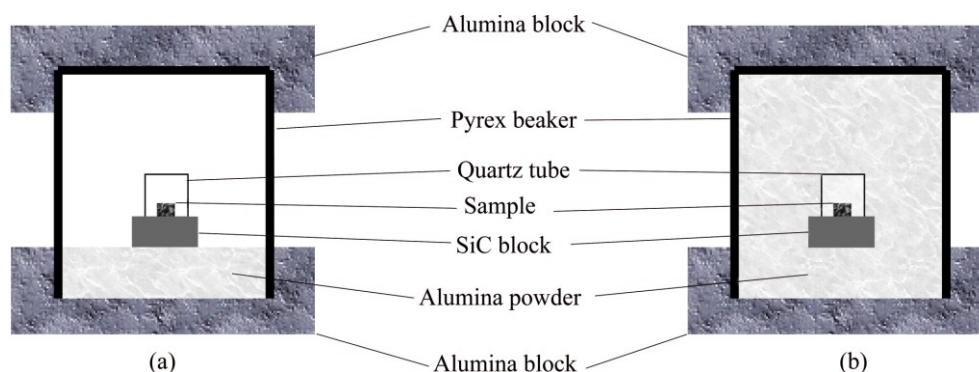


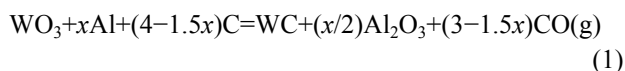
Fig. 1 Schematic illustration of experimental setup: (a) Before modification; (b) After modification

of some powders were studied by means of a scanning electron microscope (SEM: TESCAN-VEGA II).

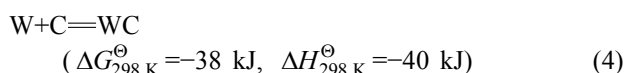
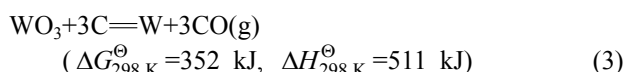
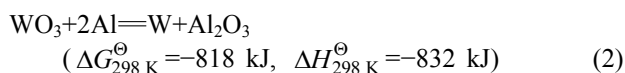
### 3 Results and discussion

#### 3.1 Thermodynamic aspects

Microwave heating is a non-equilibrium process, due to high heating/cooling rates. Thermodynamic calculations of non-equilibrium processes are not completely understood; nevertheless, using conventional thermodynamic calculations could give a useful general view about the probable reactions. The overall chemical reaction in  $\text{WO}_3\text{--Al--C}$  mixture could be presented as



In fact, Reaction (1) is the combination of the following sub-reactions:



Aluminothermic reduction reaction of  $\text{WO}_3$  (Reaction (2)) is highly exothermic [6,28]; therefore, it is rational to assume that the released heat can probably activate the reaction between  $\text{WO}_3$  and C (Reaction (3)) in the  $\text{WO}_3\text{--Al--C}$  mixture. Since Reaction (3) is endothermic [4], it is expected that simultaneous reduction of  $\text{WO}_3$  by Al and C would decrease the overall system temperature and can possibly prevent the  $\text{W}_2\text{C}$  formation.

Table 1 shows  $\Delta G_{298\text{ K}}^\ominus$ ,  $\Delta H_{298\text{ K}}^\ominus$  and  $T_{\text{ad}}$  values of Reaction (1) for some Al amounts in the range of  $1 \leq x \leq 2$ .

As shown in Table 1, for a mixture containing 2 mol of Al, standard free energy ( $\Delta G_{298\text{ K}}^\ominus$ ) has a large negative value (−856 kJ), showing a high possibility and

Table 1  $\Delta G_{298\text{ K}}^\ominus$ ,  $\Delta H_{298\text{ K}}^\ominus$  and  $T_{\text{ad}}$  values of possible reactions in various  $\text{WO}_3\text{:}x\text{Al}\text{:}(4-1.5x)\text{C}$  mixtures according to Reaction (1)

$x$	$\Delta G_{298\text{ K}}^\ominus / \text{kJ}$	$\Delta H_{298\text{ K}}^\ominus / \text{kJ}$	$T_{\text{ad}} / \text{K}$
2	−856	−872	3900
1.7	−680	−671	3240
1.4	−505	−470	2510
1.32	−458	−416	2320
1.21	−394	−342	2320
1.1	−330	−268	1940
1.06	−306	−242	1800
1	−271	−201	1570

appetite for the reaction [29]. For this sample, the reaction is highly exothermic ( $\Delta H_{298\text{ K}}^\ominus = -872\text{ kJ}$ ), thus, the heat of the reaction could change the temperature of the bulk mixture. Our calculations (see Table 1) revealed that  $T_{\text{ad}}$  of  $\text{WO}_3\text{:}2\text{Al}\text{:C}$  mixture is about 3900 K, which is much higher than Merzhanov's criterion [12]. Hence, from thermodynamic viewpoint, it is anticipated that a SHS reaction would occur during microwave heating of this mixture. As shown in Table 1, with decreasing the amount of Al in  $\text{WO}_3\text{:}x\text{Al}\text{:}(4-1.5x)\text{C}$  mixture, values of  $\Delta G_{298\text{ K}}^\ominus$  and  $\Delta H_{298\text{ K}}^\ominus$  have increased, which means a lower reaction tendency and a lower exothermicity of the system. Lower exothermicity would bring about a lower adiabatic temperature.

Regarding Table 1, the limit of Al amount by which exothermicity of Reaction (1) is high enough to meet the Merzhanov's criterion, is around 1.06 mol. It is worth noticing that  $T_{\text{ad}}$  has remained constant when  $1.21 \leq x \leq 1.32$ . This is supposed to be due to the melting of  $\text{Al}_2\text{O}_3$  in the product.

#### 3.2 Experimental findings

Table 2 shows the composition of all investigated mixtures together with the types of occurred reactions. Types of reactions were identified by visual observation.

**Table 2** Types of reactions in all investigated samples of this study (Physical phenomena, i.e., flushing and inflaming of samples, were considered as signs of SHS reactions)

$x$	2	1.7	1.4	1.1
Type of reaction	SHS	SHS	SHS	Gradual

When  $x=2$ , Reaction (1) would be as follows:

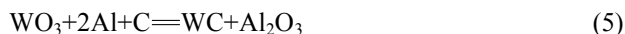
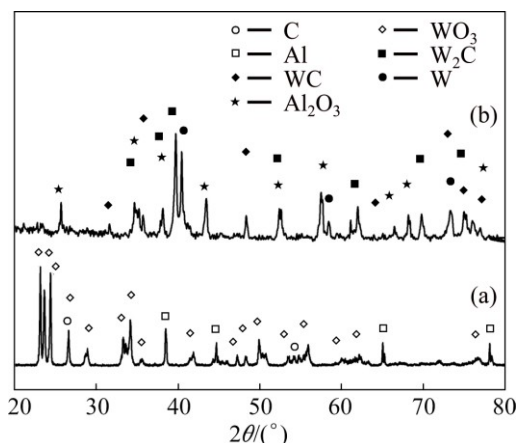
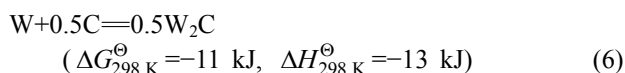


Table 2 shows that the type of reaction for a  $\text{WO}_3:2\text{Al}:\text{C}$  mixture (i.e., Reaction (5)) is SHS. This finding is in a good agreement with thermodynamic predictions as well as Merzhanov's criterion. Figure 2 represents the XRD patterns of  $\text{WO}_3:2\text{Al}:\text{C}$  mixture before and after microwave heating.

**Fig. 2** XRD patterns of  $\text{WO}_3:2\text{Al}:\text{C}$  system: (a) Starting mixture; (b) Heated by using setup in Fig. 1(a) until occurrence of SHS reaction [23]

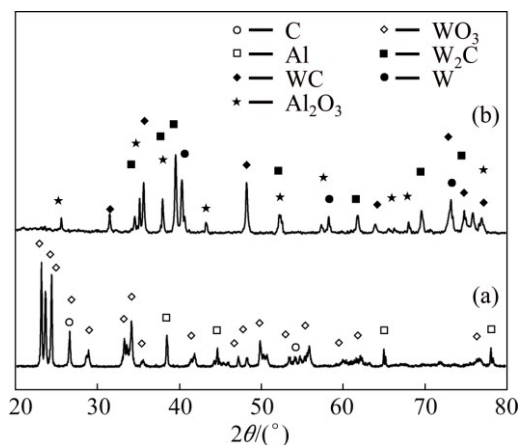
As shown in Fig. 2, XRD pattern has completely changed due to the occurrence of a SHS reaction, and no peak of the starting reagents is visible in Fig. 2(b). The presence of alumina peaks reveals that reduction of  $\text{WO}_3$  by Al has occurred. Although merely formation of  $\text{WC}:\text{Al}_2\text{O}_3$  compounds during microwave heating of  $\text{WO}_3:2\text{Al}:\text{C}$  mixture is anticipated (see Reaction (5)), the product consists of unwanted  $\text{W}_2\text{C}$  phase. Properties of  $\text{W}_2\text{C}$  phase are inferior to those of WC; hence, its formation is undesirable. We have shown earlier that the presence of  $\text{W}_2\text{C}$  phase is presumably due to 1) occurrence of carbon loss (see Reaction (6)) as the consequence of carbothermic reduction of  $\text{WO}_3$  [30] and/or 2) high thermodynamic stability of  $\text{W}_2\text{C}$  compound at high obtained temperatures [6,7].



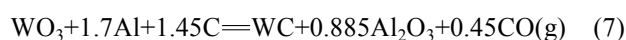
Both phenomena 1 and 2 are promoted by high temperatures resulted from intensively exothermic reduction reaction of  $\text{WO}_3$  by Al.

Based on the above justification, decrease of the systems maximum temperature to the extent that WC phase is thermodynamically stable is helpful for the production of  $\text{WC}-\text{Al}_2\text{O}_3$  composite free from  $\text{W}_2\text{C}$  compound. For this purpose, in this research work, the amount of C in the  $\text{WO}_3:2\text{Al}:\text{C}$  system has been increased in expense of Al, in accordance with Reaction (1).

Figure 3 shows the XRD patterns of  $\text{WO}_3:1.7\text{Al}:1.45\text{C}$  sample before and after microwave heating.

**Fig. 3** XRD patterns of  $\text{WO}_3:1.7\text{Al}:1.45\text{C}$  system: (a) Starting mixture; (b) Heated by using setup in Fig. 1(a) until occurrence of SHS reaction

Abrupt change of XRD pattern together with the observation of ignition phenomenon (see Table 2) confirms the thermodynamic prediction and shows that the type of occurred reaction is SHS. Table 1 shows that by decreasing the amount of Al from 2 to 1.7 mol, calculated  $T_{\text{ad}}$  of the system has decreased accordingly. Hence, a decrease in thermodynamic stability of  $\text{W}_2\text{C}$  phase is anticipated. A comparison between Fig. 2(b) and Fig. 3(b) reveals that this prediction is true, so by lower amount of Al in the initial mixture, relative share of WC phase in the products has been increased. Figure 3(b) also shows no peaks of the starting reagents in the XRD pattern of the heated sample. Since the amount of Al in the  $\text{WO}_3:1.7\text{Al}:1.45\text{C}$  mixture has not been sufficient for the reduction of entire  $\text{WO}_3$  in the mixture, the absence of  $\text{WO}_3$  peaks in Fig. 3(b) indicates that in this system, carbothermic reduction reaction has also occurred (Reaction (3)) alongside the aluminothermic reduction. Hence, the overall reaction could be written as follows:

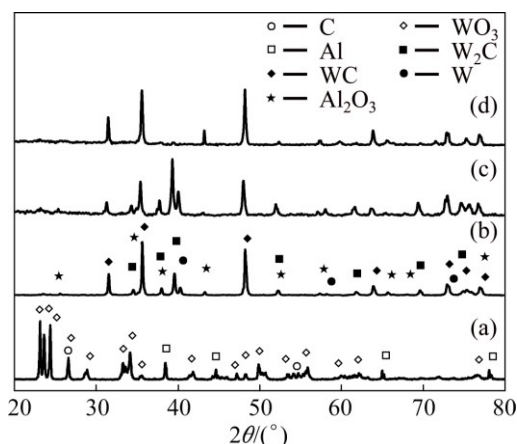


The presence of  $\text{W}_2\text{C}$  peaks in Fig. 3(b) indicates that more Al decrease is necessary for better elimination of  $\text{W}_2\text{C}$  phase from the product.

Figure 4 shows the XRD patterns of  $\text{WO}_3:1.4\text{Al}:1.9\text{C}$  sample before (Fig. 4(a)) and after (Fig. 4(b))



microwave heating.



**Fig. 4** XRD patterns of  $\text{WO}_3\text{:}1.4\text{Al:}1.9\text{C}$  system: (a) Starting mixture; (b) Heated by using setup in Fig. 1(a) until occurrence of SHS reaction; (c) Heating by using setup in Fig. 1(a), was continued after SHS moment for 10 min; (d) Heating, by using setup in Fig. 1(b), was continued after SHS moment for 10 min

Sudden change of XRD pattern and observation of ignition phenomenon (see Table 2) show that the type of occurred reaction is SHS. As mentioned before, the absence of peaks of  $\text{WO}_3$  phase in Fig. 4(b) shows that  $\text{WO}_3$  is reduced by Al and C simultaneously, according to the following reaction:

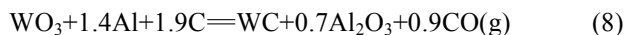


Table 1 shows that by decreasing Al from 1.7 to 1.4 mol, the calculated  $T_{\text{ad}}$  has decreased accordingly which can promote the stability of WC [6,7]. The comparison of Figs. 2(b), 3(b) and 4(b) shows that this prediction is true and with less Al in the initial mixture, WC phase in the products has become more pronounced. However, peaks of  $\text{W}_2\text{C}$  compound are still observed in Fig. 4(b). Hence, lower amount of Al should be used in the initial mixture.

XRD patterns of  $\text{WO}_3\text{:}1.1\text{Al:}2.35\text{C}$  sample before and after microwave heating are presented in Fig. 5.

With regard to thermodynamic calculations (Table 1) the reaction in this system (Reaction (9)) is feasible and it is a SHS type.

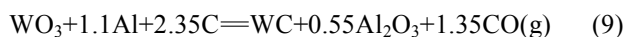
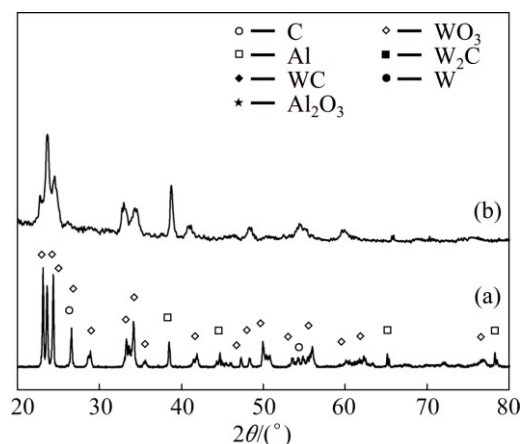
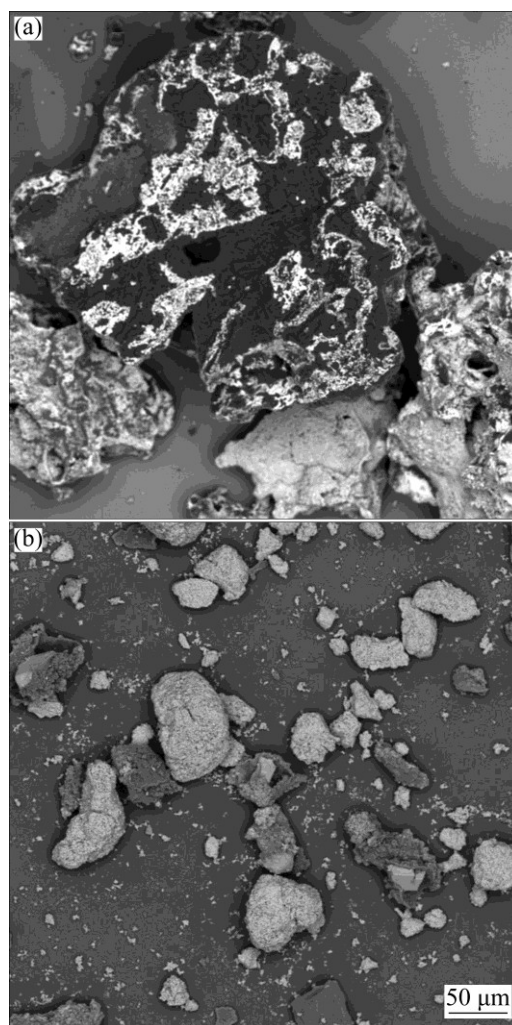


Figure 5(b) shows that peaks of the starting reagents remain in the XRD pattern of heated  $\text{WO}_3\text{:}1.1\text{Al:}2.35\text{C}$  mixture. This phenomenon together with no sign of ignition during heating (see Table 2) indicates that despite thermodynamic predictions, the type of reaction has been gradual reaction. The change of type of reactions in  $\text{WO}_3\text{:}x\text{Al:}(4-1.5x)\text{C}$  mixtures from SHS to gradual reaction, as a consequence of Al decrease, can

also be concluded from SEM results. Figures 6(a) and (b) show SEM images of  $\text{WO}_3\text{:}1.4\text{Al:}1.9\text{C}$  and  $\text{WO}_3\text{:}1.1\text{Al:}2.35\text{C}$  mixtures, respectively.



**Fig. 5** XRD patterns of  $\text{WO}_3\text{:}1.1\text{Al:}2.35\text{C}$  system: (a) Starting mixture; (b) Heated by using setup in Fig. 1(a) for 2 min

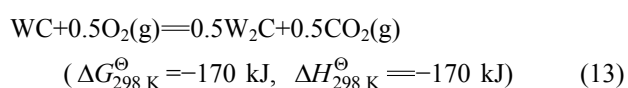
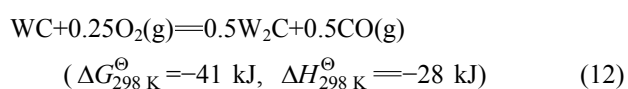
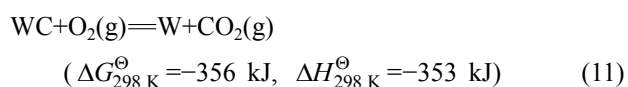
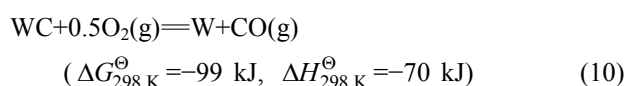


**Fig. 6** BSE-SEM images of heated  $\text{WO}_3\text{:}1.4\text{Al:}1.9\text{C}$  (a) and  $\text{WO}_3\text{:}1.1\text{Al:}2.35\text{C}$  (b) mixtures (Formation/absence of dense agglomerates are the signs of occurrence of SHS/gradual reactions in the mixtures)

Figure 6 reveals that when the type of reaction is SHS (e.g.,  $\text{WO}_3\text{:}1.4\text{Al:}1.9\text{C}$  mixture), the product contains coarse and dense agglomerates due to partial fusion and coalescence of particles at high system temperatures; while due to low system temperatures during gradual reactions, there is no possibility for such phenomenon to take place and the particles remain separated (see Fig. 6(b)). The change of type of reaction from SHS to a gradual mode is supposed to be related to the fact that high amount of C in  $\text{WO}_3\text{:}1.1\text{Al:}2.35\text{C}$  mixture decreases the contact between Al and  $\text{WO}_3$  particles, by its locating between Al and  $\text{WO}_3$ . This, in turn, lowers the rate of aluminothermic reduction of  $\text{WO}_3$ . Therefore, heat accumulation in the mixture will be diminished, which leads to the occurrence of a gradual reaction.

Our experimental results showed that the critical amount of Al in  $\text{WO}_3\text{:}x\text{Al:}(4-1.5x)\text{C}$  mixture by which the type of reaction changes from SHS to gradual mode, is about 1.3 mol. The rate of material synthesis through gradual reactions is lower than that through SHS ones [10]; so longer time is required for the fabrication of the same final product. Since our experimental setup was not confidentially sealed against oxygen penetration into the reaction chamber for a long time, only SHS reactions were believed to be reliable. Therefore, a lower limit of  $x \geq 1.4$  was set. With regard to Figs. 2(b), 3(b) and 4(b), the highest amount of WC phase is obtained with a  $\text{WO}_3\text{:}1.4\text{Al:}1.9\text{C}$  mixture. However, some amount of unwanted  $\text{W}_2\text{C}$  phase is observed in the product (see Fig. 4(b)). Further elimination of  $\text{W}_2\text{C}$  was expected to be possible by continuation of microwave heating after the occurrence of SHS reaction, as it was proposed in our previous work [23].

The XRD pattern of  $\text{WO}_3\text{:}1.4\text{Al:}1.9\text{C}$  mixture heated for 10 min is shown in Fig. 4(c). This pattern shows that by heating continuation, amounts of W and  $\text{W}_2\text{C}$  phases have increased. This phenomenon could possibly be attributed to the penetration of some amount of oxygen into the reaction chamber which could decompose WC phase according to the following reactions:

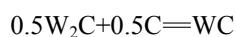


In order to increase the protection efficiency of the experimental setup against air penetration, the following modifications were made:

1) Sufficient amount of alumina powder was added into the inner space of Pyrex beaker (see Fig. 1(b)) to act as an air penetration barrier.

2) Additional amount of carbon (30%, mole fraction) was added to the  $\text{WO}_3\text{:}1.4\text{Al:}1.9\text{C}$  mixture. So, when some oxygen (as air) passes through the alumina layer, it will react with the additionally used carbon.

XRD pattern of  $\text{WO}_3\text{:}1.4\text{Al:}1.9\text{C}$  mixture heated for 10 min by employment of the modified setup, is shown in pattern Fig. 4(d). The comparison of Figs. 4(b) and (d) reveals that in the latter case,  $\text{WC-Al}_2\text{O}_3$  composite powder has been synthesized successfully. This shows that use of alumina barrier layer together with additional carbon amount in the mixture provides a good solution to the oxygen penetration problem, so W and  $\text{W}_2\text{C}$  phases (see Fig. 4(b)) can convert to WC through Reactions (4) and (14), respectively.



$$(\Delta G_{298\text{ K}}^\ominus = -27\text{ kJ}, \Delta H_{298\text{ K}}^\ominus = -27\text{ kJ}) \quad (14)$$

## 4 Conclusions

1) The amount of Al ( $x$ ) in the  $\text{WO}_3\text{:}x\text{Al:}(4-1.5x)\text{C}$  mixture has a considerable effect on the reaction tendency for occurrence ( $\Delta G^\ominus$ ), reaction exothermicity ( $\Delta H^\ominus$ ) and  $T_{\text{ad}}$  values of the system.

2) When  $1.4 \leq x \leq 2$ , the type of reaction is found to be SHS. It is also found that at  $x \leq 1.3$ , the reaction type changes to a gradual mode, which brings about incompleteness of reaction and remaining some initial reagents in the product.

3) The occurrence of SHS/gradual reaction can be recognized by observation of the presence/absence of large and dense agglomerates in the heated products, which is an indirect scale of the system heat release as well as the reaction type, consequently.

4) For mixtures with a SHS type ( $1.4 \leq x \leq 2$ ) reaction, the products would consist of unwanted  $\text{W}_2\text{C}$  phase and  $\text{WO}_3$  is reduced by Al and C simultaneously. By decreasing the system temperature through partial substitution of Al with C, the amount of  $\text{W}_2\text{C}$  phase in the product decreases considerably.

5) Although in  $\text{WO}_3\text{:}1.4\text{Al:}1.9\text{C}$  mixture, WC is the main obtained phase,  $\text{W}_2\text{C}$  phase is also found in the product. A complete elimination of  $\text{W}_2\text{C}$  phase can be achieved by continuation of microwave heating after the occurrence of SHS reaction, together with applying necessary modification to the experimental setup for confidential prevention of oxygen penetration into the

reaction chamber.

6) A good consistency was found between the thermodynamic predictions and experimental results.

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## 以 $\text{WO}_3\text{-Al-C}$ 混合物为原料 采用简易微波辅助法制备 $\text{WC-Al}_2\text{O}_3$ 复合粉末

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**摘 要:** 提出一种操作简单、成本低廉的制备  $\text{WC-Al}_2\text{O}_3$  复合粉末的方法。热力学计算表明,  $\text{WO}_3\cdot x\text{Al}\cdot(4-1.5x)\text{C}$  混合体系中  $\text{WO}_3$  在铝热还原反应过程放出大量的热量, 促进了此体系中的碳热还原反应(吸热反应)。用碳原子部分取代铝原子阻止了副产物  $\text{W}_2\text{C}$  的形成, 这是由于它在较低温度下具有较低的热力学稳定性。为验证本文作者所提出的反应机理, 在微波炉中对不同  $\text{WO}_3\cdot x\text{Al}\cdot(4-1.5x)\text{C}(1.1\leq x\leq 2)$  混合物进行热处理。结果表明, 当  $1.4\leq x\leq 2$  时, 反应类型为自蔓延高温合成反应,  $\text{WO}_3\cdot x\text{Al}\cdot(4-1.5x)\text{C}$  混合体系中少量 Al 导致大量 WC 的产生; 当混合体系中  $x=1.4$  mol 时, 体系经过自蔓延高温合成反应后, 在密封环境下连续进行微波加热能获得不含  $\text{W}_2\text{C}$  的  $\text{WC-Al}_2\text{O}_3$  复合物; 当  $x\leq 1.3$  时, 由于反应不完全以及剩余的反应物, 上述反应变得缓慢。

**关键词:** 微波加热; 燃烧合成;  $\text{WC-Al}_2\text{O}_3$  复合物

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