

[Article ID] 1003- 6326(2001) 04- 0513- 04

Evolution of recrystallization textures in high voltage aluminum capacitor foils^①

LIU Chur-ming(刘楚明)¹, ZHANG Xin-ming(张新明)¹, ZHOU Hong-zhang(周鸿章)²,
CHEN Zhi-yong(陈志永)¹, DENG Yun-lai(邓运来)¹, ZHOU Zhuo-ping(周卓平)¹

(1. Department of Materials Science and Engineering, Central South University,
Changsha 410083, P. R. China;

2. Northeast Light Alloy Co. Ltd., Harbin 150060, P. R. China)

[Abstract] The evolution of recrystallization textures in high voltage aluminum capacitor foils which are produced with a high level of cold reduction was tracked by analysis of microstructure and crystallographic texture. The results show that the deformation textures are mainly composed of S-orientation, Cu-orientation and a little B_s-orientation. During the low temperature stages of final annealing, the iron precipitates first along the sub-grain boundaries, and the Fe concentration in the matrix becomes low. Then, the cube grains nucleate preferably into the sub-grains. At high temperature stages, the cube nuclei can grow preferably because of their 40° <111> orientation relationship to the S orientation, the main component of the rolling texture. Finally, the cube texture is sharply strong and the R orientation is very weak in the foils.

[Key words] aluminum capacitor foils; deformation textures; recrystallization textures

[CLC number] TG 111.7

[Document code] A

1 INTRODUCTION

The capacitance of electrolytic capacitors depends on the effective surface of aluminum foils from which they are made^[1]. The effective surface can be greatly increased by up to two orders of magnitude through an etching process that forms narrow channels along the crystallographic <001>-direction into the foils. Since this "tunnel etching" follows the crystallographic <001>-direction, a strongly textured material consisting only cube-oriented grains is favourable and therefore the aim of the processing. The cube texture in cold rolled high purity aluminum foils developed by recrystallization is mainly influenced by trace elements^[2], hot rolling processing^[3], final cold rolling reduction^[4], heat treatment^[5] and impurity contents^[6], and so on.

And the work by Suzuki et al.^[6] demonstrated that the several factors were considered the origin of the suppression of the development of textures such as the existence of precipitates, clusters, and solute atoms. And the concentration of solute atoms in the matrix is the dominant factor, which has a strong influence on recrystallization behavior. In this paper we investigated the evolution of the recrystallization textures of high voltage aluminum capacitor foils during the final multi-stage annealing.

2 EXPERIMENTAL

In the present investigation a DC cast slab with the dimensions of 450 mm × 1 000 mm × 5 000 mm of

high purity Al (99.99%) was used; the impurities present in that material are given in Table 1. After a homogenization treatment for 20 h at 600 °C, the slab was reheated to 520 °C and held at this temperature for 2 h. Then the material was hot-rolled on a reversing breakdown mill to 16 mm thickness, and then hot-finishing-rolled to 7 mm thickness with an exit temperature of 310 °C. The hot band was reversibly cold rolled with a thickness reduction of as much as 98% to a final thickness of 0.11 mm. Finally, the cold rolled specimens were annealed in a vacuum furnace at 200 °C for 3 h plus 520 °C for 2 h.

Table 1 Chemical composition of investigated aluminum (mass fraction, %)

chromium (mass fraction, %)				
Fe	Si	Cu	Mg	
0.001 0	0.000 8	0.003 3	0.001 9	
Mn	Zn	Ti	Ni	Al
< 0.002	< 0.002	< 0.002	< 0.002	Bal.

For a microstructural characterization of the cold rolled and recrystallized foils TEM was employed. The crystallographic textures were determined by measuring four incomplete pole figures {111}, {200}, {220}, {311} by means of fully automatic X-ray diffractometer using CuK_α radiation. The experimental orientation distribution functions (ODF) $f(g)$ were computed according to Bunge's series expansion method^[7]. All ODFs were ghost corrected by using Gauss-type scattering functions^[8]. In order to combine the information on the concurrent evolution

① **[Foundation item]** Project (1999064908) supported by the National Key Fundamental Researches for Development; Project (97053316) supported by the Doctoral Foundation of State Education Ministry of China

[Received date] 2000- 11- 22; **[Accepted date]** 2001- 02- 22

of microstructure and texture during rolling and annealing, the EBSD was employed.

3 RESULTS AND DISCUSSION

3.1 Experimental results

Fig. 1 gives the $\{111\}$ pole figure, ODF and β -fibre of cold rolled foils in thickness of 0.11 mm. It shows that the deformation textures of high purity aluminum are mainly composed of S -orientation $\{123\} \langle 634 \rangle$, Cu -orientation $\{112\} \langle 111 \rangle$ and B_s -orientation $\{110\} \langle 112 \rangle$. But the densities of Cu -orientation and B_s -orientation are very weak. The $\{111\}$ pole figure and ODF of Al foils recrystallized at 200 °C for 3 h plus 500 °C for 2 h are shown in Fig. 2. The cube texture develops strongly, and the R orientation is very weak.

Fig. 3 shows a cube-oriented nucleus and its diffraction pattern of the foils annealed at 200 °C for

3 h according to TEM. Fig. 4 exhibits the appearance of precipitates which formed along the subgrain boundaries at low temperature stage of final annealing. Fig. 5 shows the completely recrystallized cube-oriented grains which are separated by approximately planar grain boundaries.

3.2 Discussion

It is known that the recrystallization textures are influenced by deformation texture^[9], annealing temperature, heating rate^[10], amount of iron in solution, and so on. But the origin of recrystallization textures during annealing of a deformed metal has been a matter of controversy for decades, with the discussion focusing on the rival theories^[11], oriented nucleation and oriented growth. The oriented nucleation is assumed that the nuclei possess preferred orientations which by their growth will determine the texture. The oriented growth is assumed that a broad spe-

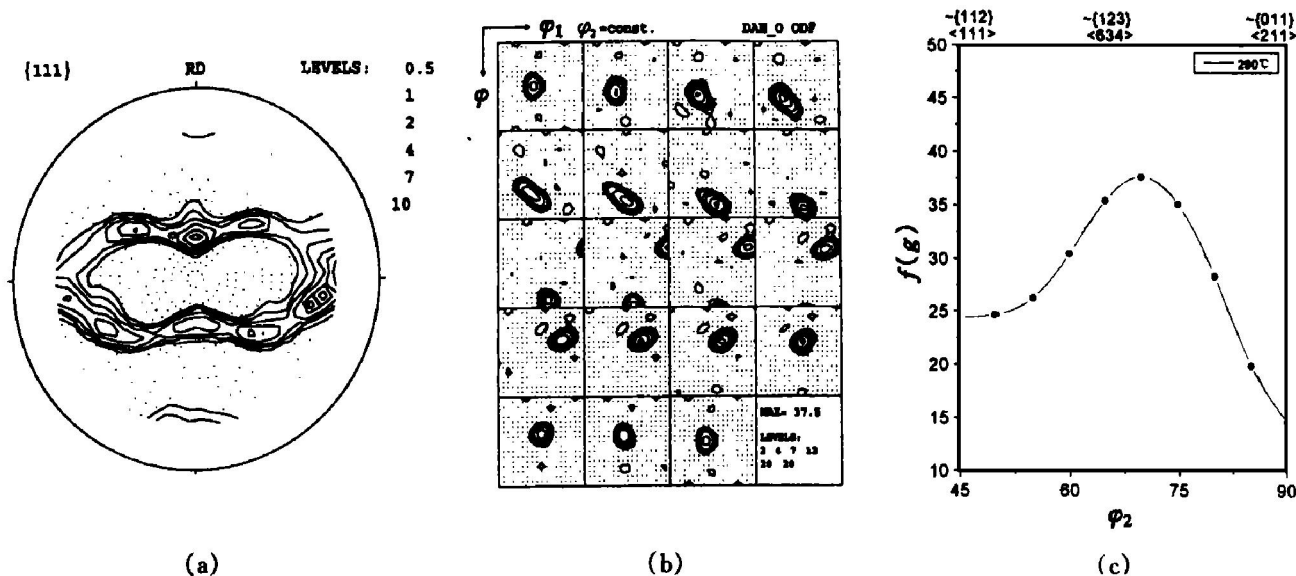


Fig. 1 $\{111\}$ pole figure (a) and ODF (b) and β -fibre (c) for samples 0.11 mm in thickness ($\epsilon = 98\%$)

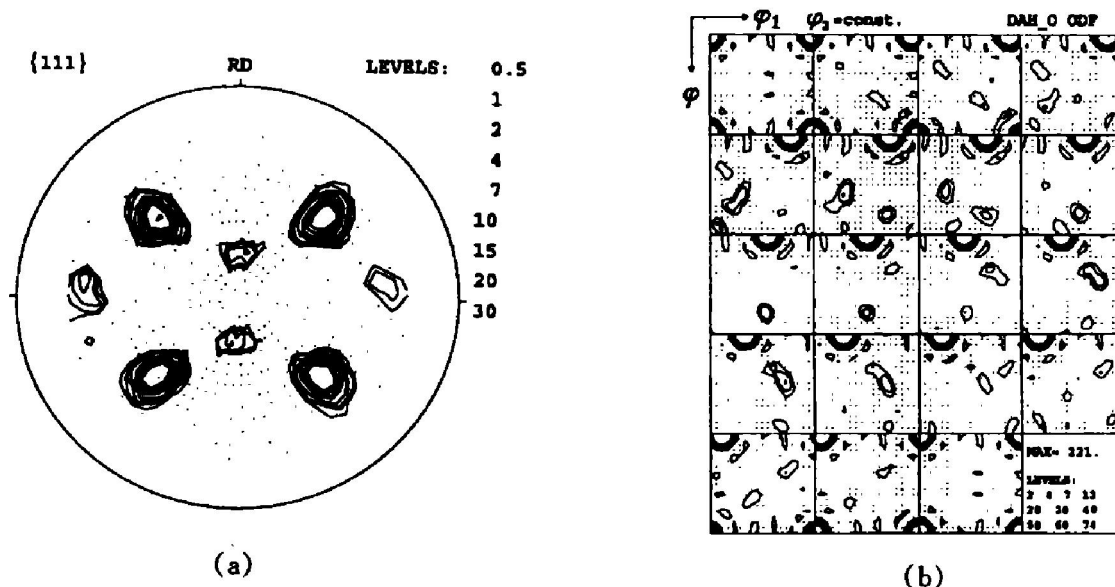


Fig. 2 $\{111\}$ pole figure (a) and ODF (b) for samples 0.11 mm in thickness after final annealing

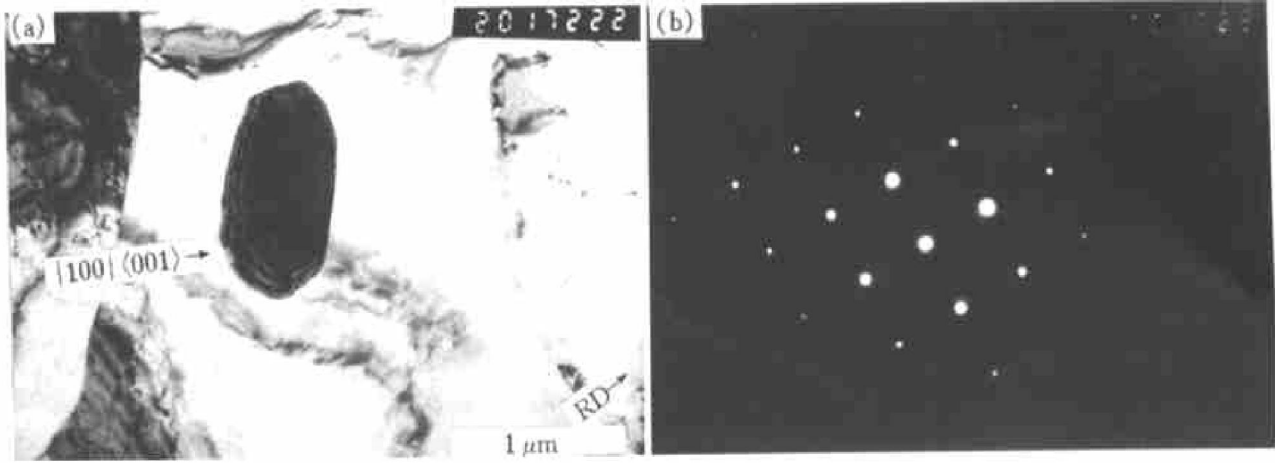


Fig. 3 Micrograph and diffraction pattern of cube nucleus
(a) —A cube-oriented nucleus annealing at 200 °C for 3 h;
(b) —Diffraction pattern taken at the cube-oriented nucleus with a arrow

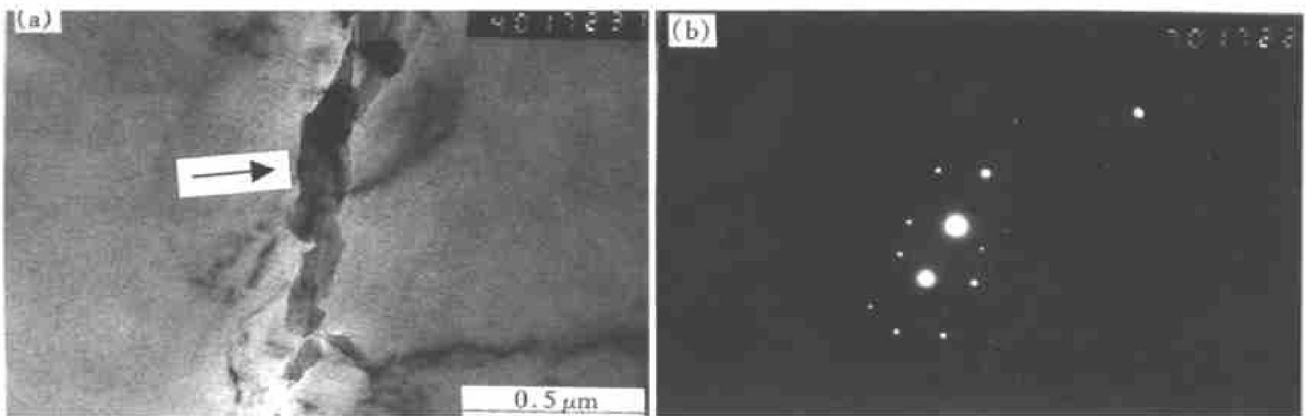


Fig. 4 Microstructure with precipitates along subgrain boundaries (a)
and diffraction pattern taken at the precipitate with a arrow (b)

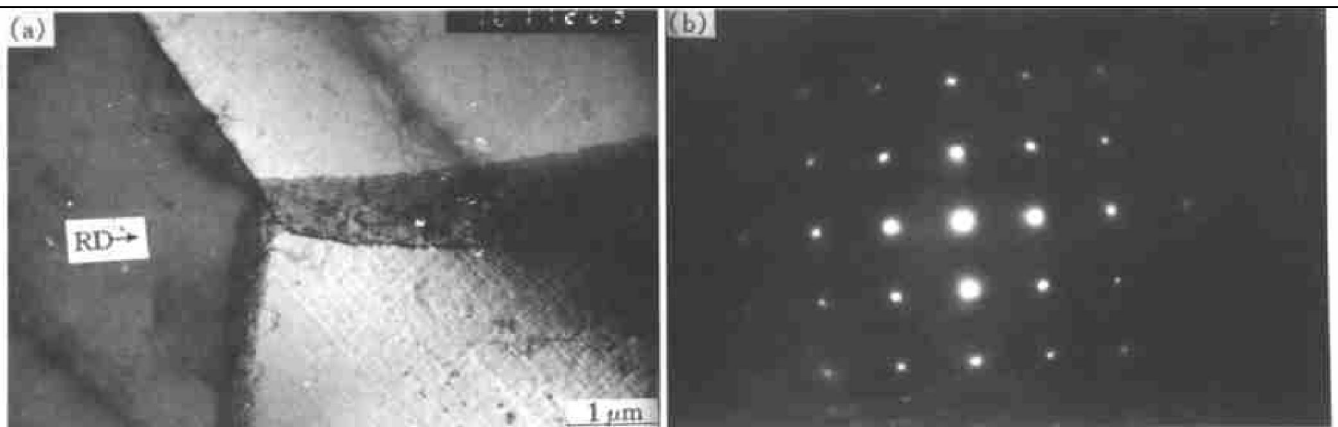


Fig. 5 TEM micrograph (a) and diffraction pattern (b) of recrystallized grains with cube orientation
(Annealed at 200 °C for 3 h plus 520 °C for 2 h after 98% cold rolling reduction)

etrum of nucleus orientations is formed, and those with the best growth conditions with respect to the surrounding deformed matrix will determine the recrystallization texture. In Al, the cube texture is interpreted as nucleating in transition bands formed during preceding deformation. And the nuclei with a $40^\circ \langle 111 \rangle$ orientation relationship to the neighbouring deformation matrix were found to possess an especial-

ly high growth rate^[12].

The presence of cube-oriented bands in the heavily deformed material is of importance to the question whether the cube recrystallization texture is developed by oriented nucleation or oriented growth. Cube-oriented grains presumably nucleate in cube bands that persist in the as-deformed state. TEM micrograph illustrating the formation of cube-oriented nu-

clei at low temperature stage of the final annealing is shown in Fig. 3(a). At the same time some precipitates are observed in Fig. 4(a). The Al-Fe equilibrium diagram shows that with the low iron content of the investigated material probably only FeAl_3 particles are present. The particles are not uniformly distributed as they display a tendency to cluster along the grain boundaries. Because the Fe concentration in the matrix becomes low, no dissolved or a little iron hinders the formation of the cube orientation. And the cube texture is formed so long as the Fe content in solution is sufficiently small. These precipitates explain why cube-oriented nuclei arise during the low temperature stage of final annealing^[13].

The work by Ito et al.^[5] demonstrated that the dissolved iron hinders the formation of any genuine recrystallization and thus leads to the retaining of the rolling orientation, i. e. the R-orientation. The dissolved iron hinders the formation of the cube orientation but not that of the R-orientation by genuine recrystallization. In the present case, at low temperature stage of final annealing indeed very fine precipitates and cube-oriented nuclei have been observed respectively in TEM (Fig. 3(a) and Fig. 4(a)) and then the cube-oriented nuclei can grow preferably by discontinuous grain growth due to their $40^\circ \langle 111 \rangle$ orientation relationship to the S orientation which is a main component of rolling texture at high recrystallization temperature^[14]. Whereas the driving force for recrystallization is provided by the lattice defects, in particular the dislocation stored in the as-deformed substructure during the preceding cold rolling deformation, grain growth is driven by the reduction in grain boundary area.

4 CONCLUSIONS

The nucleation sites are of primary importance and it has been found that the initial cube-oriented deformation bands within the original grains are preferential sites for recrystallization cube orientation nuclei in high purity aluminium (99.99%), deformed 98% by cold rolling. At low final annealing temperatures where most of the dissolved iron is precipitated before recrystallization, the cube-oriented nuclei can form. This is because the dissolved iron hinders the formation of the cube grains more strongly than that of the R-grains. And at high annealing temperatures the strong growth of the cube orientation could be due to the lack of dissolved iron and because of their $40^\circ \langle 111 \rangle$ orientation relationship to the S orientation. Finally, the cube texture sharply increases and the R orientation is suppressed in the foils.

ACKNOWLEDGEMENTS

The authors express their best thanks to Dr. SHEN Jian of Beijing General Research Institute for Nonferrous Metals in China and Institute für Metallphysik der RWTH Aachen in Germany for their help in experiments.

[REFERENCES]

- [1] Engler O, Moor-Young H. Evolution of the cube texture in high purity aluminum capacitor foils by continuous recrystallization and subsequent grain growth [J]. *Materials Science and Engineering*, 1999, A271: 371– 381.
- [2] LIU Chir-ming, ZHANG Xir-ming, CHEN Zhi-yong, et al. Effect of trace yttrium on cube texture of high purity aluminum foils [J]. *Trans Nonferrous Met Soc China*, 2001, 11(2): 222– 225.
- [3] LIU Chir-ming, ZHANG Xir-ming, CHEN Zhi-yong, et al. The effect of hot finishing rolling on cube texture in high purity aluminum foils [J]. *Trans Nonferrous Met Soc China*, 2001, 11(1): 103– 107.
- [4] Hasenclever J, Scharf G. Evolution of Microstructure and texture in Al 99/99-foils for high voltage electrolytic capacitors [A]. *Proceedings of the 5th International Conference ICAA5* [C]. Grenoble, France, 1996. 565 – 570.
- [5] Ito K, Lücke K, Rixen R. The influence of pre-annealing and annealing temperatures on the recrystallization textures of cold rolled aluminium-iron alloys [J]. *Z Metallkde*, 1976, 67(5): 338– 347.
- [6] Suzuki T, Arai K, Shiga M, et al. Impurity effect on cube texture in aluminum foils [J]. *Metallurgical Transactions A*, 1985, 16A: 27– 36.
- [7] Bunge H J. *Mathematische Methoden der Textur Analyse* [M]. Akademie Verlag, Berlin, 1969.
- [8] MAO Weimin, ZHANG Xir-ming. *Quantitative Texture Analysis of Crystalline Materials* [M]. Beijing: Metallurgical Industry Press, 1995.
- [9] Lee D N. The evolution of recrystallization textures from deformation textures [J]. *Scripta Metallurgica et Materialia*, 1995, 32(10): 1689– 1694.
- [10] Rogers D H, Roberts W T. Rolling textures in aluminium sheet [J]. *Z Metallkde*, 1974, 65(2): 100– 105.
- [11] Lücke K, Engler O. Effect of particles on development of microstructure and texture during rolling and recrystallisation in fcc alloys [J]. *Materials Science and Technology*, 1990, 6(11): 1113– 1130.
- [12] Nes E, Vante H E. The $40^\circ \langle 111 \rangle$ orientation relationship in recrystallization [J]. *Z Metallkde*, 1996, Bd87 (6): 448– 453.
- [13] Ito K, Musick R, Lücke K. The influence of iron content and annealing temperature on the recrystallization textures of high purity aluminium-iron alloys [J]. *Acta Metall*, 1983, 31(12): 2137– 2149.
- [14] Hjeln J, Ørsund R, Nes E. On the origin of recrystallization textures in aluminum [J]. *Acta Metall Mater*, 1991, 39(7): 1377– 1404.

(Edited by YUAN Sai-qian)