

[Article ID] 1003- 6326(2001) 04- 0492- 04

## Stress-induced deformation at $A_p \sim M_p$ and thermal cycling behavior of Cu-Al-Ni single crystals<sup>①</sup>

CHEN Qing-fu(陈庆福)<sup>1,2</sup>, CAI Wei(蔡伟)<sup>1</sup>, ZHAO Lian-cheng(赵连城)<sup>1</sup>  
(1. School of Materials Science and Engineering, Harbin Institute of Technology,

Harbin 150001, P. R. China;

2. Department of Materials and Chemical Engineering, Liaoning Institute of Technology,  
Jinzhou 121001, P. R. China)

**[Abstract]** Stress-induced deformation in  $A_p \sim M_p$  and concomitant shape recovery behavior of Cu-13.4Al-4.0Ni single crystals were studied. Abnormal high stress-induced deformation exists in  $A_p \sim M_p$  under the conditions of either heating with load or cooling with load. The recovered deformation is successively composed of four parts, the recoveries from superelasticity, normal reverse transformation, thermally activated reverse transformation of partially stabilized martensite and reverse transformation of stabilized martensite by over-heating. With increasing cycling number, the recovery part from normal reverse transformation decreases, while that from reverse transformation of stabilized martensite by over-heating increases, which shows a typical stabilization of martensite.

**[Key words]** CuAlNi single crystal; stress-induced deformation; two way shape memory; superelasticity; stabilization of martensite

**[CLC number]** TG 139; TG 111

**[Document code]** A

### 1 INTRODUCTION

In the past two decades much attention has been paid to the study of Cu-Al-Ni shape memory alloys<sup>[1~7]</sup>. Results show that the alloys have relatively good phase stability<sup>[8]</sup>, good aging stability<sup>[9]</sup> and high superelasticity<sup>[10, 11]</sup>. In the research of superelasticity and training for obtaining two way memory effect<sup>[12]</sup>, it was found that when the post-quenched single crystal was cooled for the first time from a temperature above  $A_f$  with load through the transformation temperature range of  $A_p \sim M_p$  ( $A_p$  and  $M_p$  represent respectively the peak temperature from austenite to martensite and from martensite to austenite measured by DSC<sup>[9]</sup>), there was an extremely high strain peak in the strain-temperature curve. Therefore it would be of engineering importance to study the stability of the strain, corresponding superelasticity and relationships between strain and temperature. Based on the previous work, the authors study the stress-induced deformation in the temperature range of  $A_p \sim M_p$  and thermal cycling behavior of Cu-Al-Ni single crystals.

### 2 EXPERIMENTAL

The alloy used was single crystal with a composition of Cu-13.4Al-4.0Ni (mass fraction, %). The dimension of the specimen for stress-induced deformation

measurement was  $d$  3 mm  $\times$  200 mm. After being heated at 800 °C for 20 min and then quenched into water at room temperature, the transformation temperatures of the specimen measured by DSC<sup>[9]</sup> were  $M_s = 96$  °C,  $M_p = 84$  °C,  $M_f = 60$  °C;  $A_s = 73$  °C,  $A_p = 96$  °C and  $A_f = 102$  °C. The axial direction of the sample was close to  $\langle 001 \rangle$  of  $\beta$  phase at high temperature. The deformation and thermal cycling tests were carried out with the apparatus described in Ref. [13], by which the parameters of temperature, stress and time can be logged, monitored and processed by computer. A thermocouple (with precision of 0.1 °C) was connected directly with the sample and the temperature was adjusted by the combination of oil bathing, resistance heating, water-cooling coil and a stirring element. The temperature range measured was 60~178 °C. The tensile stress was applied at precision of 1 N. The strain measurement was made by a LVDT (Linear Variable Differential Transformer) that connected with the sample by quartz rods, and the precision was 2  $\mu$ m. The gauge length was 100 mm. Both the loading and unloading speed were 73 MPa/min.

Enough experimental data<sup>[9~12]</sup> showed that there was a difference between the temperatures measured by DSC and the real actuating temperatures of the single crystal. Although the transformation temperature ranges of  $M_s \sim M_f$  and  $A_s \sim A_f$  measured by DSC were quite wide, the actual shape memory temperatures were generally at the sharp narrow tempera-

① **[Foundation item]** Project (990821108) supported by the Scientific Research Fund of Liaoning Education Bureau

**[Received date]** 2000- 10- 10; **[Accepted date]** 2000- 12- 04

tures near  $M_p$  and  $A_p$  respectively, which might be caused by the great differences in the dimensions and the volume constraint conditions (for example very small flake, small disc or bulk) of the sample. Therefore, it might be reasonable to express both the transformation behavior and the real actuating temperature of the shape memory by together using of  $M_s$ ,  $M_p$  and  $A_s$ ,  $A_p$  respectively, from the engineering point of view.

Considering the fact that the transformation temperatures were above room temperature and the sample was heated from room temperature, we set the measuring temperature at 87 °C (in the range of  $M_p \sim A_p$ ). Before the occurrence of main reverse transformation at 87 °C, the stress was applied and released and then thermally cycled so as to study the relationships among stress, strain and temperature.

### 3 RESULTS AND DISCUSSION

#### 3.1 Shape memory effect in $A_p \sim M_p$

Fig. 1 shows the strain—temperature relationship at different stages of thermomechanical cycling. Through thermal cycling, for the post-quenched Cu-Al-Ni single crystal in 50~136 °C in the initial two thermal cycles, the obtained two way shape memory effect is only about 0.20%, which occurs at 92~100 °C and its actuating temperatures correspond well with  $M_p$  and  $A_p$  measured by DSC. When the sample is loaded ( $p = 87.8$  MPa) at a temperature of ( $M_f - 20$  °C), a deformation of 0.35% is produced due to martensite reorientation and this deformation recovers in the next heating process. When the sample is loaded ( $p = 48.1$  MPa) at temperature of ( $A_f + 20$  °C) and cooled with the load to ( $M_f - 20$  °C) and unloaded, followed by thermal cycling between ( $M_f - 20$  °C) and ( $A_f + 20$  °C), it was found that in the first cooling cycle from ( $A_f + 20$  °C) with load, a very high stress induced deformation (7%) is pro-

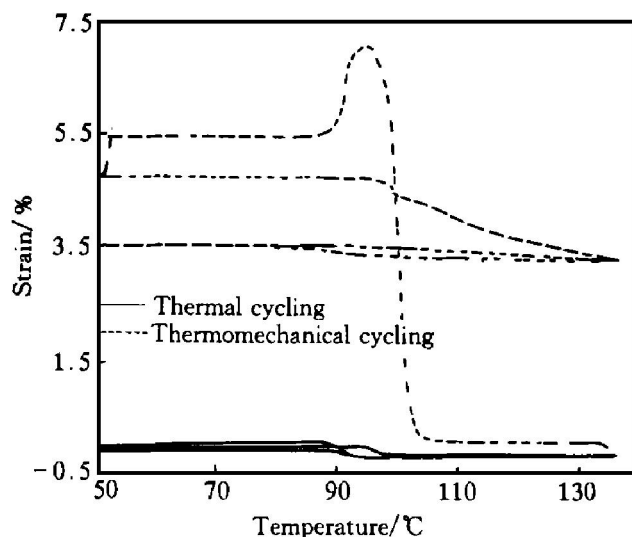


Fig. 1 Stress—temperature curve at different stages

duced in  $A_p \sim M_p$ . Another experiment<sup>[12]</sup> also proves that when the post-quenched single crystal sample is loaded ( $p = 120.3$  MPa) for the first time at temperature below  $M_f$ , 3% deformation is produced by martensite reorientation; and when heating with the load a stress-induced deformation is further produced in  $M_p \sim A_p$ , which makes the total deformation up to 6%.

#### 3.2 Stress-induced deformation between $A_p$ and $M_p$ and characteristics of recovery

Normally the practical application stress of Cu-Al-Ni alloy is no more than 100 MPa, so a stress of 72.2 MPa is loaded at 87 °C as testing stress in following experiments.

Figs. 2(a) and (b) show respectively the strain—temperature curve and stress—strain curve around 87 °C in the first cycle. After the stress is applied, a total deformation of 3.98% is produced at around 87 °C, and this stress-induced strain typically linearly increases with stress, as shown in Fig. 2(b). Its mechanism is that some of the same kind variants in parent phase gradually start to form martensite in the single crystal<sup>[1]</sup>. By releasing the stress there is a superelastic recovery of 0.41%. The rest deformation

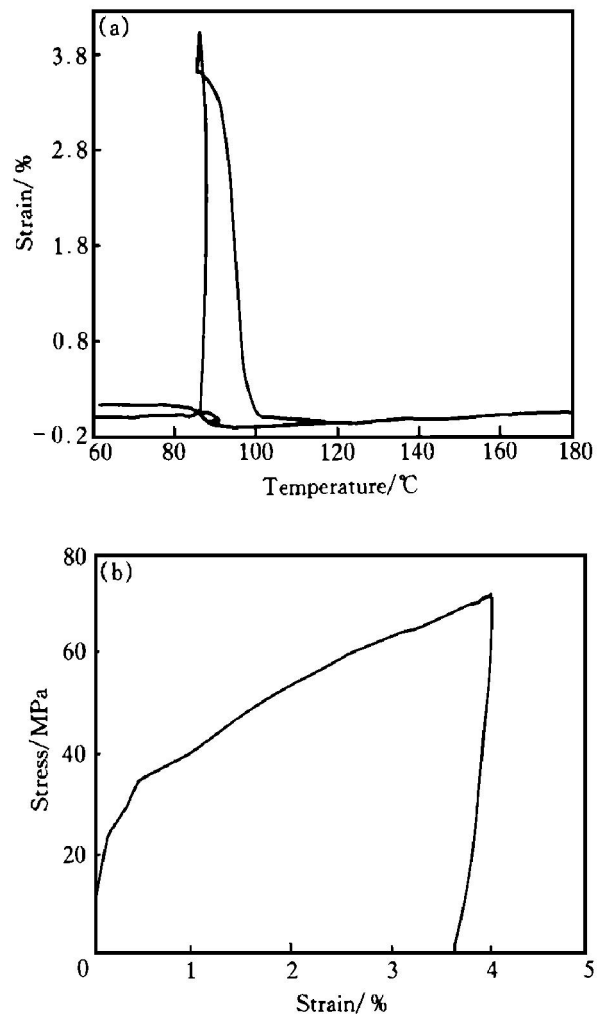


Fig. 2 Strain—temperature (a) and stress—strain (b) curves around 87 °C in first cycle

is almost recovered in the regular reverse transformation temperature range of 87~102 °C.

The above stated deformation behavior and its recovery characteristics change greatly with cycling going on. Figs. 3(a) and (b) show respectively the strain—temperature and strain—stress curves around 87 °C in the 7th cycle. By comparing these with results in Fig. 2, it can be seen that although the total stress-induced deformation at 87 °C by applying stress of 72.2 MPa is almost 4%, the deformation component is changed gradually from the typically linear to nearly plateau-like. The corresponding start plateau stress is lowered gradually, and the corresponding strain increases gradually with the cycling number. The mechanism can be rooted in the easy start of individual variant of the same kind variants to form martensite in the single crystal with the cycling going on. The total shape recovery in every stress-thermal cycle is composed of the following four parts, as indicated in Fig. 3(a) by mark 1, 2, 3 and 4, respectively:

$$\varepsilon = \varepsilon_e + \varepsilon_{\text{sate}} + \varepsilon_t + \varepsilon_{\text{stab}} \quad (1)$$

where  $\varepsilon_e$  is superelastic recovery upon the release of stress, and it increases gradually with the cycling

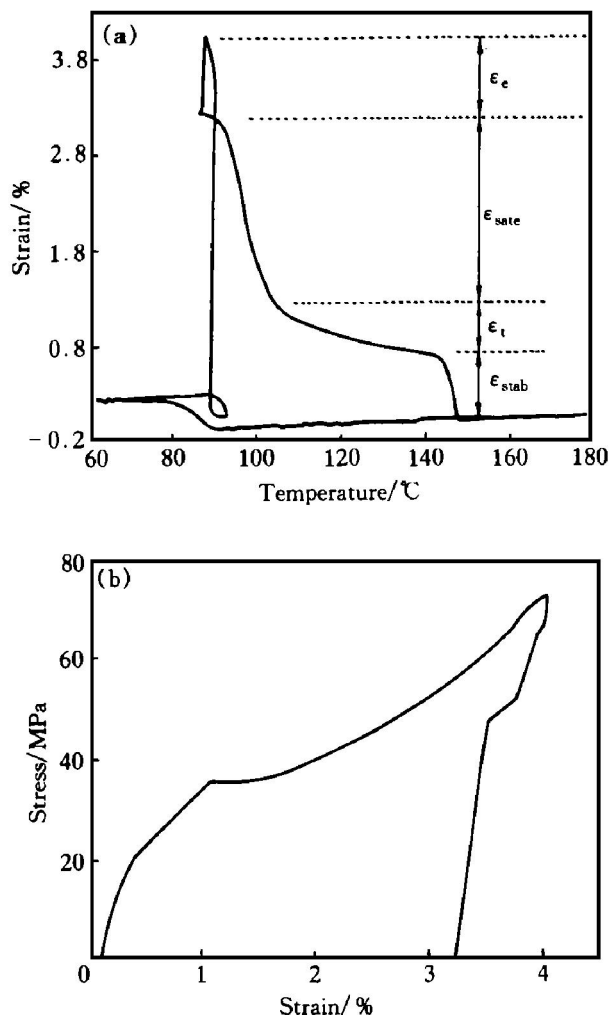


Fig. 3 Strain—temperature (a) and stress—strain (b) curves around 87 °C in 7th cycle

number within a certain stress limit<sup>[14]</sup>. The recovery process after unloading can be divided into the following three reverse transformation parts of different mechanisms.  $\varepsilon_{\text{sate}}$  can be regarded as reverse transformation of stress assisted transformation effect (SATE) which occurs normally at 87~102 °C, and it decreases with the stress-thermal cycling; the part of  $\varepsilon_t$  can be regarded as the thermally activated reverse transformation of partially stabilized martensite; the part of  $\varepsilon_{\text{stab}}$  can be regarded as the reverse transformation of stabilized martensite in the overheating process, and it increases with the stress-thermal cycling<sup>[15]</sup>. Experimental results prove that for every fixed training stress the corresponding reverse transformation temperature of  $\varepsilon_{\text{stab}}$  is almost the same. In Fig. 3(a), the reverse transformation temperature of stabilized martensite caused by applying stress of 72.2 MPa around 87 °C is 146 °C.

### 3.3 Two way memory effect

Fig. 4 shows the strain—temperature curves of the first and the 8th thermal cycle after trained for 13 cycles with stress of 72.2 MPa around 87 °C. It can be noted that the two way memory effect is increased to 0.4%, and such two way memory effect after training is very sensitive to temperature at  $A_p \sim M_p$

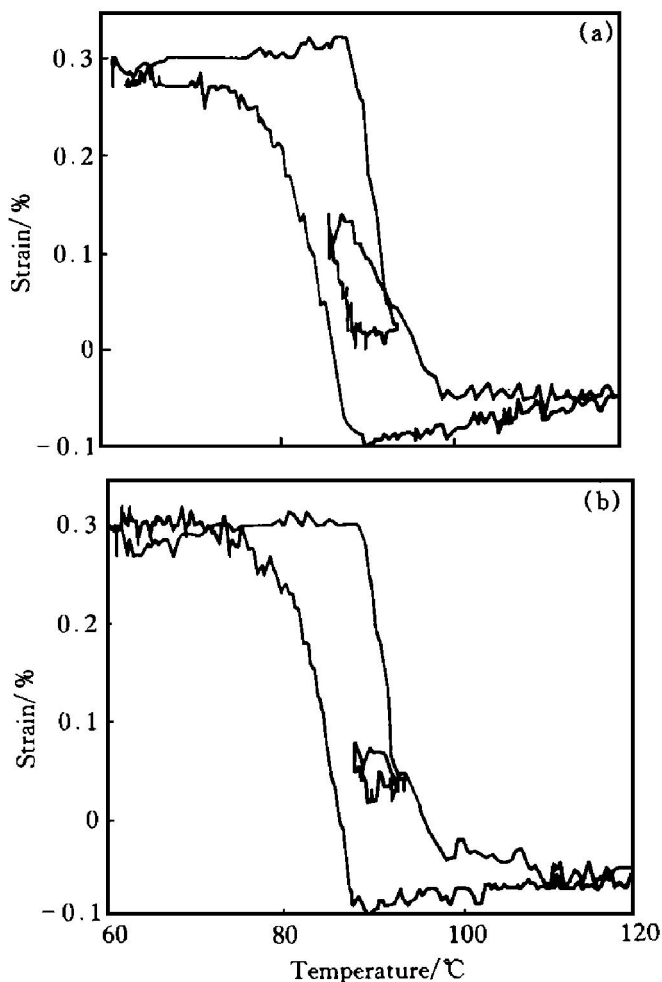


Fig. 4 Strain—temperature curves after trained for 13 cycles  
(a) —In first thermal cycling; (b) —In 8th thermal cycling

(84~ 96 °C). If the reverse shape recovery temperature is lowered at the stage of incomplete recovery, there is a forward shape change due to forward transformation, which likes the partial (or incomplete) two way memory effect within a very narrow temperature range in NiTi alloy<sup>[16]</sup>. When the temperature is further increased, the reverse transformation continues. It is found by comparing the curves in Figs. 4(a) and (b) that the obtained two way memory effect is relatively stable. Even the sample subjected to thermal cycling for 8 times at temperature up to ( $A_f + 76$  °C), the loss of two way shape memory is little.

#### 4 CONCLUSIONS

1) Abnormal high stress-induced deformation phenomena exists at  $A_p \sim M_p$  under the condition of either heating with load or cooling with load to the studied Cu-Al-Ni single crystals.

2) The recovered deformation is successively composed of four parts of recoveries from superelasticity, normal reverse transformation, thermally activated reverse transformation of partially stabilized martensite and reverse transformation of stabilized martensite by over-heating.

#### [ REFERENCES ]

- [ 1 ] Otsuka K, Wayman C M, Nakai K, et al. Superelasticity effect and stress-induced martensitic transformations in CuAlNi alloys [ J ]. *Acta Metallurgica*, 1976, 24: 207–226.
- [ 2 ] Otsuka K, Sakamoto H, Shimizu K. Successive stress-induced martensitic transformations and associated transformation pseudoelasticity in CuAlNi alloys [ J ]. *Acta Metallurgica*, 1979, 27: 585–601.
- [ 3 ] Sakamoto H, Shimizu K. Effect of heat treatment on thermally formed martensite phases in monocrystalline CuAlNi shape memory alloy [ J ]. *JISI International*, 1989, 29(5): 395–404.
- [ 4 ] Morris M A, Lipe T. Ductility and two way memory effect associated with stress-induced martensite stability produced by deformation of CuAlNi alloys [ A ]. *Proc of the Intern Conf on Martensitic Transformation* [ C ]. Monterey, California, USA, 1992. 1033–1038.
- [ 5 ] Picornell C, Rapacioli P, Pons J, et al. Two way shape memory effect in CuAlNi single crystals [ J ]. *Materials Science and Engineering*, 1999, A273–275: 605–609.
- [ 6 ] Cingolani E, Arneodo Larochette P, Ahlers M. The two way memory effect: influence of stabilization in single and polycrystals of Cu-based alloys [ J ]. *Materials Science Forum*, 2000, 327–328: 453–456.
- [ 7 ] LOU M Z, YANG S L, WAN B B W, et al. Shape memory effect of Cu-11.9Al-6.43Mn alloy [ J ]. *The Chinese Journal of Nonferrous Metals*, 2000, 10(3): 323–325.
- [ 8 ] Cingolani E, van Humbeeck J, Ahlers M. Stabilization and two way shape memory effect in CuAlNi single crystals [ J ]. *Metallurgical and Materials Transactions A*, 1999, 30A(3): 493–499.
- [ 9 ] CHEN Q F, ZHAO L C, Stalmans R, et al. Effect of preaging on the transformation temperatures of CuAlNi single crystals [ J ]. *J Materials Science and Technology*, 2000, 8(2): 94–100.
- [ 10 ] CHEN Q F, ZHAO L C, Stalmans R, et al. Influence of isothermal treatment on superelastic behavior of Cu-13.8Al-4.0Ni (mass fraction) single crystals [ J ]. *J Mater Sci Technol*, 2001, 17(1): 49–50.
- [ 11 ] CHEN Q F, ZHAO L C, Stalmans R, et al. Superelastic behavior and stabilization of stress-induced martensite in Cu-13.4Al-4.0Ni single crystals [ J ]. *Trans Nonferrous Met Soc China*, 2001, 11(2): 161–165.
- [ 12 ] CHEN Q F, ZHAO L C, Stalmans R, et al. Methods for obtaining two way memory effect and stressed two way memory effect of CuAlNi single crystals [ J ]. *Trans Nonferrous Met Soc China*, 2001, 11(1): 10–17.
- [ 13 ] Stalmans R, van Humbeeck J, Delaey L. Thermomechanical cycling, two way memory and concomitant effects in CuZnAl alloys [ J ]. *Acta Metall Mater*, 1992, 40(3): 501–511.
- [ 14 ] CHEN Q F, ZHAO L C, Stalmans R, et al. Superelastic behavior of CuAlNi single crystals at different phase status [ J ]. *Journal of Harbin Institute of Technology*, 2000, 25(5): 116–119.
- [ 15 ] Qingfu C, Hurdato I, Stalmans R, et al. Stabilization of martensite during training of CuAlNi single crystals [ J ]. *J de Physique*, 1995, C–2: 181–186.
- [ 16 ] Khusainov M A, Belyakov V N. General mechanism of loop formation of hysteresis in incomplete interval of transformation [ A ]. *Proc of the 2nd Intern Conf on Shape Memory and Superelastic Technologies* [ C ]. Asilomar, Pacific Grove, California, USA, 1997. 207–213.

( Edited by YANG Bing )