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Thermodynamics of Cu(II)-NH₃-NH₄CH₂O system¹

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Abstract: The thermodynamics of a complex solution system, Cu(II)-NH₃-NH₄Cl+H₂O, was presented both theoretically and experimentally. Firstly, according to the principles of simultaneous equilibrium and aqueous electronic charge neutrality of the system, a nonlinear mathematical thermodynamic model with multi-members was set up. In this model, there were six unknowns: pH value, concentration values of free Cl⁻, free NH₃, total concentration values of Cu²⁺, Cl⁻ and NH₃, four equilibrium equations and three equilibrium equations of total quantum of Cu²⁺, Cl⁻ and NH₃, as well as an equilibrium equation of electric charge, were involved in the model. Then after specifying the values of total concentrate of NH₃ and Cl⁻, the model was solved precisely using MATLAB language, and the other four unknowns were obtained. According to the values obtained above, various valuable figures regarding thermodynamic relation of the system were protracted also with MATLAB, including two and three dimensions figures. These figures and data can supply the theoretic conference for optimizing the ratio of leaching reagents in copper extraction through ammonia hydrometallurgy. Finally, the solubility of CuO were measured in the system of NH₃-NH₄Cl+H₂O. The results show that the model and the thermodynamic data obtained are reliable.

Key words: copper hydrometallurgy; ammoniacal ammonium leaching; metal complex; thermodynamic model; MATLAB language

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1 INTRODUCTION

Ammonia metallurgy has the merits of a high leaching rate, good selectivity, easy purification process, so until now it was still studied in a great area^[1-4]. We have previously studied on the thermodynamics in the systems of Zn(II)-NH₃- $(NH_4)_2 SO_4 - H_2 O^{[5]}, Zn(II) - NH_3 - (NH4)_2 CO_3 H_2O^{[6]}$ and $Zn(II)-NH_3-NH_4CI-H_2O^{[7]}$ and discovered the rules of zinc solubility in these systems. The former two systems were used to supple the theoretic basis for producing the high grade zinc oxide^[8] from zinc oxide materials. While the third system was used to supple the theoretic basis for producing high purity zinc. As for ammonia copper metallurgy, the system of Cu-NH₃-H₂O has been studied thoroughly. While the system of Cu-NH₄Cl-H₂O has been studied in the way of construction of φ —pH figure^[9]. However, at first, the paper did not discover the rules of the equilibrium solubility of copper in the system; in addition, it supposed the concentration of Cu^{2+} , Cl⁻ and NH₃ were certain values. Thus, the results in the study were limited. At last, the method of construction of φ -pH figure is not suitable in studying the system of Cu-NH₄Cl-H₂O, because the potential of the system is actually a constant, the pH value of this system varies from 6 to 12,

and more over, it is very difficult to adjust pH value of the system. Actually, it is more suitable to use the method of construction of the concentrate figure of $c(\operatorname{Cu}^{2+})-c(\operatorname{NH4Cl})-c(\operatorname{NH4OH})$.

As the development of using ammoniacal ammonium chloride metallurgy to treat copper oxide ore^[10,11], to clarify the thermodynamics of this system becomes more and more exigent.

In this paper, at first, according to the principles of simultaneous equilibrium and aqueous electronic charge neutrality of the system, a nonlinear mathematical thermodynamic model with multimembers was set up. In addition, the model was solved precisely through programming with MAT-LAB language. Thirdly, according the values obtained, various valuable figures of thermodynamic relation of the system were protracted also with MATLAB language, and the character of the system was discussed. At last, a series of experiments were carried out to show the reliability of the model and the thermodynamic data.

2 THERMODYNAMIC ANALYSIS AND MODEL CONSTRUCTION

Actually, the species such as $CuNH_3(OH)^+$, $CuNH_3(OH)_3^-$ and $Cu(NH_3)_2(OH)_{2(aq)}$ could only be produced when the pH value was very high. In this system, the pH value was kept in the range of 6.0^- 12. 5. So these species were ignored in this thermodynamic model. While for the species such as $CuCl_{2(aq)}$, $CuCl_3^-$ and $CuCl_4^{2-}$, their stable constants were very small in the ammonia systems, so these species were also ignored in our thermodynamic model.

On the base of the simultaneous equilibrium principle, every copper complex is equilibrium with the copper oxide at the present of copper oxide in the system:

$$CuO + iNH_{3} + H_{2}O = Cu(NH_{3})_{i}^{2+} + 2OH^{-}$$
(1)

$$CuO + (i-1)H_{2}O = Cu(OH)_{i}^{2-i} + (i-2)H^{+}$$
(2)

$$CuO + H_{2}O + iCI^{-} = CuCl_{i}^{2-i} + 2OH^{-}$$
(3)

According to the exponential computation method^[12, 13] and supposing that the activity of each species is equal to the mole concentration of itself, the concentration of these species can be expressed as

$$c(\mathbf{R}) = \exp(A + B \bullet \mathbf{pH} + C \bullet \ln c(\mathbf{NH}_{3(aq)}) + D \bullet \ln c(\mathbf{Cl}^{-}))$$
(4)

where $c(\mathbf{R})$ is every species mole concentration; A is the constant calculated from equilibrium constants or thermodynamic data; B stands for the multiplication of ln10 and gained or lost proton number; C indicates the numbers of ammonia ligand; while D stands for the number of chloride ligand.

The critical stability constants of copper complexes, presented in Table 1, were chosen from Ref. [14]. The thermodynamic data, presented in Table 2, were chosen from Ref. [15].

There are altogether three solid phases in this system, CuO, Cu(OH) $_{2(s)}$ and Cu(OH) $_{1.5}$ Cl_{0.5(s)}.

For Cu(OH) $_{2(s)}$, the analytical expression of the equilibrium concentration of Cu²⁺ is as follows:

 $c(Cu^{2+})_{1} = \exp(20.9535 - 4.606 \cdot pH)$ (5)

While for CuO, the analytical expression of the equilibrium concentration of Cu^{2+} is as follows:

 $c(Cu^{2+})_2 = exp(16.9250 - 4.606 \cdot pH)$ (6)

Thus, the equilibrium concentration of Cu^{2+} with $Cu(OH)_{2(s)}$ in this system is always larger than the equilibrium concentration of Cu^{2+} with CuO. This means that the equilibrium solubility of $Cu(OH)_{2(s)}$ is larger than that of CuO. Put it in another way, in the whole leaching process of CuO, no Cu(OH)_{2(s)} can be presented in this system. So, in this certain thermodynamic model,

 Table 1
 Critical stability constants of copper complexs at 298 K

copper complexs at 298 K								
Complex $\lg \beta_i$		Complex	$\lg\beta_i$					
$CuCl^+$	0.4	Cu(OH) 2(aq)	12.8					
Cu(NH ₃) ²⁺	4.12	Cu(OH) 3	14.5					
Cu(NH ₃) $_{2}^{2+}$	7.63	Cu(OH) ²⁻ / ₄	15.6					
Cu(NH ₃) $_{3}^{2+}$	10.51	$CuNH_3(OH)^+$	14.9					
$Cu(NH_3)_4^{2+}$	12.6	CuNH3(OH)3	16.3					
Cu(NH ₃) $\frac{2}{5}$ ⁺	12.43	$Cu(NH_3)_2(OH)_{2(aq)}$	15.7					
Cu(OH) ⁺	6.3							

Table 2Gibbs free energy ofrelated species at 298 K (J/mol)

10	-	<u>5 at 270 K (j/ 1110</u>	/
Species	${\vartriangle}G^{\ominus}$	Species	ΔG^{\ominus}
N H 3(aq)	- 75 322	Cu ²⁺	65 490
NH_{4}^{+}	- 79 333	$CuO_{(s)}$	- 129 642
N H 3(aq)	- 26 712	$NH_{4}Cl_{(aq)}$	- 210 522
Species	${\vartriangle}G^{\ominus}$	Species	$\mathrm{p}K$ $_{\mathrm{sp}}$
H ₂ O	- 237 065	Cu(OH) _{2(s)}	18.9 ^ª
H^{+}	0	Cu(OH) 1.5 Cl _{0.5(s)}	17.16 ^ª
0H-	- 157 899		

Cu(OH)_{2(s)} was not considered.

While as for Cu(OH) $_{1.5}\,Cl_{0.5(s)}$, the analytical expression of the equilibrium concentration of Cu^{2+} is as follows:

 $c(Cu^{2+})_{3} = \exp(8.8435 - 3.4545 \cdot pH - 0.5 \cdot lnc(Cl^{-}))$

For compare the size of $c(Cu^{2+})_3$ and $c(Cu^{2+})_2$, an inequation is constructed:

 $\ln c(\operatorname{Cu}^{2+})_{3} - \ln c(\operatorname{Cu}^{2+})_{2} = - 8.0815 +$

1. 151 5 • pH - 0. 5 •
$$\ln c(C\Gamma) < 0$$
 (8)

(7)

Thus, when the above inequation (8) is true, the phase of Cu(OH)_{1.5} Cl_{0.5(s)} would exist in the system, while otherwise, when inequation (8) is not true, CuO would be the only solid phase. After solving the inequation, it is found that only when pH < 7.0 and $c(Cl^-) > 2.718$, the inequation come into existence. But, the results of solving the model when CuO is the only solid phase showed that only in pure NH₄Cl solution can the equilibrium pH value be smaller than 7.0. This means that Cu(OH)_{1.5}Cl_{0.5(s)} would only exist in a very limited range. Thus, for simplifying the process of solving the model, CuO is looked as the only solid phase existing in the system.

Using the data in Table 2, the values of A, B, C and D in Eqn. (4) can be calculated and listed in Table 3.

Table 3	Constants in exponential Eqn. (1) for						
calculating species concentration							

Species	A	В	С	D
Cu ²⁺	16.925 0	- 4.606	0	0
$CuCl^+$	17.846	- 4.606	0	1
$Cu(NH_3)^{2+}$	26. 411 7	- 4.606	1	0
Cu(NH ₃) $^{2+}_{2}$	34. 493 7	- 4.606	2	
Cu(NH ₃) $^{2+}_{3}$	41. 125 2	- 4.606	3	0
Cu(NH ₃) $_{4}^{2+}$	45.9376	- 4.606	4	0
Cu(NH ₃) $_{5}^{2+}$	45.5461	- 4.606	5	0
$\mathrm{N}\mathrm{H}\mathrm{4}^{+}$	21.427	- 2.303	1	0
H^{+}	- 32.2348	2.303	0	0
OH-	0	- 2.303	0	0

According to the principle of substance quantity changeless, the sum concentration of copper, ammonia and chloride can be expressed as Eqns. (9), (10) and (11), respectively:

$$c(\operatorname{Cu}^{2+})_{\mathrm{T}} = c(\operatorname{Cu}^{2+}) + \sum_{i=1}^{5} c(\operatorname{Cu}(\operatorname{NH}_{3})_{i}^{2+}) + c(\operatorname{Cu}^{2+})$$
(9)

$$c(\text{NH}_{3(\text{aq})})_{\text{T}} = c(\text{NH}_{4}^{+}) + c(\text{NH}_{3(\text{aq})}) + \sum_{i=1}^{5} (i \cdot c(\text{Cu}(\text{NH}_{3})_{i}^{2+}))$$
(10)

 $c(\text{Cl}^{-})_{\mathrm{T}} = c(\text{Cl}^{-}) + c(\text{Cu}\text{Cl}^{+})$ (11)

where $c(NH_{3(aq)})_T$ is the total concentration of ammonia and ammonium in the system; $c(NH_{3(aq)})$ is the concentration of free ammonia in system; *i*, *j* and *k* are the numbers of ammonia, chloride and hydroxide ligands, respectively.

According to the principle of electronic charge

neutrality, the equation of electronic charge equilibrium can be expressed as

$$2 \cdot c(Cu^{2^{+}})_{T} + c(NH4^{+}) + c(H^{+}) = c(Cl^{-})_{T} + c(OH^{-})$$
(12)

Then the model of this system can be set up as a combination of above four Equations, i. e. Eqns. (9) - (12).

3 MODEL SOLVING WITH MATLAB AND RE-SULTS AND DISCUSSION

The relation among the six variables of $c(\operatorname{Cu}^{2+})_{\mathrm{T}}$, $c(\operatorname{Cl}^{-})_{\mathrm{T}}$, $c(\operatorname{NH}_{3(\operatorname{aq}}))_{\mathrm{T}}$, $c(\operatorname{Cl}^{-})$, $c(\operatorname{NH}_{3(\operatorname{aq}}))_{\mathrm{T}}$, $c(\operatorname{Cl}^{-})$, $c(\operatorname{NH}_{3(\operatorname{aq})})$ and pH is confined by the model. If two of them are given, other four variables may be obtained from the above mentioned simultaneous equations by the computation program with MAT-LAB language compiled by ourselves.

During the actual calculating process, as the total concentration of Cl⁻ and NH_{3(aq)} is determined by the composition of the leaching reagent, so it is preferable to specify these two values, both varying from 0⁻⁵ mol/L. The calculated dissolvability of CuO in the system of Cu (II)-NH₃-NH₄Cl-H₂O is listed in Table 4.

The calculated results are also shown in Figs. 1-5.

By thorough analysis of Fig. 1, it shows that: 1) the equilibrium concentration of Cu^{2+} in a pure ammonia aqueous solution or in a pure ammonium chloride aqueous solution is very low. 2) when the ratio of $c(NH_4OH)$ to $c(NH_4Cl)$ is lower than 1, the equilibrium concentration of Cu^{2+} increases rapidly with the increasing ammonia concentration, but when the ratio is larger than 1, the equilibrium concentration of Cu^{2+} increases slowly with the increasing ammonia concentration; 3) when the ratio

Table 4 Calculated dissolvability of CuO in system of Cu(II)-NH₃-NH₄Cl-H₂O (mol/L)

	_			•	c(1	NH4OH)	х <i>Г</i>			•					
c(NH4Cl)	0	0.4	1.0	1.4	2.0	2.4	3.0	3.4	4.0	4.4	5.0				
0	8. 71 × 10 ⁻⁷	3. 09 × 10 ^{- 5}	0.00051	0.001 23	0.00281	0.004 1	0.00629	0. 007 91	0. 010 54	0. 012 43	0. 015 45				
0.4	0.000166	0. 080 158	0. 148 29	0. 166 51	0. 179 87	0. 184 81	0. 189 62	0. 191 9	0. 194 63	0. 196 18	0. 198 32				
1.0	0.000626	0. 146 3	0. 322 39	0. 390 61	0. 441 63	0. 458 48	0. 472 79	0. 478 59	0. 484 47	0. 487 28	0. 490 53				
1.4	0.001124	0. 166 31	0. 386 96	0. 495 64	0. 593 14	0. 627 12	0. 654 95	0. 665 58	0. 675 69	0.6802	0. 685 08				
2.0	0.002 205	0. 184 36	0. 439 25	0. 587 89	0. 761 43	0. 838 26	0. 906 29	0. 931 87	0. 954 84	0. 964 36	0. 973 93				
2.4	0.003164	0. 192 83	0.46022	0. 623 26	0. 833 03	0. 940 82	1. 049 2	1. 092 7	1. 131 7	1.1475	1. 162 8				
3.0	0.004 972	0. 203 03	0. 482 58	0. 658 2	0.90042	1.0419	1. 211 9	1.293	1.3723	1.4051	1. 436 2				
3.4	0. 006 431	0. 208 85	0. 494 21	0. 675 13	0. 930 19	1.0856	1. 286 9	1. 393 6	1. 508 4	1. 558 8	1.6075				
4.0	0.009007	0. 216 74	0. 508 95	0. 695 53	0. 963 14	1. 131 6	1. 363 9	1.5001	1.6672	1.7509	1.8386				
4.4	0. 010 988	0. 221 63	0. 517 63	0. 707 08	0. 980 51	1. 154 7	1.4001	1. 549 6	1.7445	1.8502	1.9693				
5.0	0. 014 362	0. 228 61	0. 529 58	0. 722 51	1.0025	1. 182 7	1. 441 5	1.6042	1. 828 4	1.9605	2. 125 3				



Fig. 1 Relationship of $c(Cu^{2+})$ with $c(NH_4OH)$ and $c(NH_4Cl)$ in Cu(II)-NH₃-NH₄ClH₂O system



Fig. 2 Relationship of $c(Cl^{-})$ with change of $c(NH_4Cl)$ and $c(NH_3(aq))$ in system of Cu(II)-NH₃-NH₄Cl+H₂O





of $c(NH_4Cl)$ to $c(NH_4OH)$ is lower than 1, the equilibrium concentration of Cu^{2+} increases rapidly with increasing ammonium chloride concentration,



Fig. 4 Relationship among pH, c(NH₄OH) and c(NH₄Cl) in system of Cu(II)-NH₃-NH₄Cl·H₂O



Fig. 5 Concentration of three main complex species of Cu²⁺ under various c(NH₄OH) and c(NH₄Cl) in system of Cu(II)-NH₃-NH₄Cl-H₂O 1 --Cu(NH₃)²⁺; 2 --Cu(NH₃)²⁺; 3 --Cu(NH₃)²⁺; 3 --Cu(NH₃)²⁺
(Concentration of other complexes of Cu²⁺ and Cu²⁺ is almost zero.)

however, when the ratio is larger than 1, the equilibrium concentration of Cu^{2+} increases slowly with the increasing ammonium chloride concentration.

From Fig. 2 it can be seen that the concentration of free Cl^- increases with the increasing ammonium chloride concentration, and the concentration of free Cl^- is almost equal to the concentration of initial ammonium chloride. This means that Cu^{2+} almost doesn't not form complex with Cl^- in this system.

Fig. 3 shows that when the ratio of $c(NH_4OH)$ to $c(NH_4Cl)$ is lower than 1, the concentration of free ammonia is almost equal to zero, while when the ratio is larger than 1, the concentration of free ammonia increases rapidly.

This means that when the ratio of $c(NH_4OH)$ to $c(NH_4Cl)$ is lower than 1, almost all of NH₃ form complexes with Cu^{2+} . While when the ratio of $c(NH_4OH)$ to $c(NH_4Cl)$ is larger than 1, free NH₃ increases rapidly.

Fig. 4 shows that the value of pH increases when the concentration of NH_4OH increases, while when the concentration of NH_4Cl increases, the value of pH decreases, and the value of pH varies from 6 to 12. 5.

Fig. 5 shows that: 1) at most of the time $Cu(NH_3)_4^{2+}$ is the domain copper complex in the system, while when $c(NH_4Cl) - c(NH_4OH) < 2$, $Cu(NH_3)_5^{2+}$ becomes the domain copper complex; 2) the sum of the concentration of $Cu(NH_3)_3^{2+}$, $Cu(NH_3)_4^{2+}$ and $Cu(NH_3)_5^{2+}$ have almost more than 99% of all copper complexes.

However, this does not mean that Cl^- has little affect on the solubility of CuO, because Fig. 1 shows that without Cl^- the solubility of CuO is almost equal to zero even if the concentration of NH₄OH increases to 5 mol/L. We think that the function of Cl^- mainly lies in neutralizing electronic charge of the solution, because a Cu(II)-ammonia complex always takes two positive electronic charge.

From above we can also find that other anions such as $SO_4^{2^-}$, NO_3^- or $CO_3^{2^-}$ can also be used to neutralizing electronic charge of the solution, and be used in leaching copper oxide ore. However, they all have some disadvantages: for $SO_4^{2^-}$, it is precipitable with Ca^{2+} , which is very abundant in the ore, and will be consumed quickly; for NO_3^- , it is easy to be reduced and volatile; as for $CO_3^{2^-}$, it is also precipitable with Ca^{2+} and Mg^{2+} , and it is also volatile. While Cl^- doesn't precipitate with Ca^{2+} and Mg^{2+} , and its volatility is relatively low. So, ammonium chloride may be the most suitable leaching reagent for copper oxide ore.

4 EXPERIMENTAL CONFORMATION

Excessive copper oxide of the analysis grade was added to the aqueous solution of ammonia and ammonium chloride at a certain concentration, then agitated for 168 h at temperature 25 °C. Finally the copper concentration of the filtered solution was analyzed. A comparison of the values of $c(Cu^{2+})T$ of experimental and theoretically calculated is shown in Figs. 6⁻8.

Fig. 6 and Fig. 7 show that: 1) the experimental values are very similar with the theoretical values under the same condition, the absolute average error between the experimental values and the theoretically calculated values of copper equilibrium concentration is 9. 63%; 2) most of the experimental values are smaller than the theoretical values



Fig. 6 Comparison of experiment $c(Cu^{2+})_T$ with theoretically calculated in system of $Cu(\Pi)$ -NH₃-NH₄ClH₂O (group 1)



Fig. 7 Comparison of experiment $c(Cu^{2+})_T$ with theoretically calculated in system of Cu(II)-NH₃-NH₄CHH₂O (group 2)

under the same condition, this may be because during experiments, the evaporation of the ammonia could not be prevented completely; 3) under most of the time, the errors between experimental and theoretical values increase when ion strength of the solution increases, this may be due to the decrease of activity of the ions, when ion strength of the solution increases.

Fig. 8 shows that when pure ammonium chloride solution is used to dissolve CuO, the errors between the experimental values and theoretical values are somewhat large. Actually, this is because that the new solid phase, $Cu(OH)_{1.5} Cl_{0.5(s)}$, is produced in this case, just as discussed before. From the phenomena of the experiments, it shows that when the concentration of ammonium chloride is higher than 3 mol/L, a white or green precipi-



Comparison of experiment $c(Cu^{2+})_T$ with Fig. 8 theoretically calculated in system of Cu(II)-NH₃-NH₄CH₂O (group 3)

tate, is produced in the conical flask. This effect would decrease the concentration of Cu²⁺ in the solution. But the second experimental point in Fig. 8 is higher than theoretic value. This may be an analysis error occuring here.

CONCLUSIONS 5

1) According to the principle of simultaneous equilibrium and the principle of aqueous electronic charge neutrality, a thermodynamic model of the system, Cu(II)-NH₃-NH₄CIH₂O, is expressed as Eqns. $(9)^{-}(12)$.

2) Through programming with MATLAB language, the above model is solved precisely and the equilibrium dissolvability of CuO in the system of Cu(II)-NH₃-NH₄Cl-H₂O is obtained.

3) Through further analysis with MATLAB language of the above data obtained, it is discovered that ammonia copper complex, such as $Cu(NH_3)_4^{2+}$ and $Cu(NH_3)_5^{2+}$, are the predominant species in this system.

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