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# Joining of SiC<sub>p</sub>/Al composites by insert powder layers<sup>10</sup>

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**Abstract:** Mixed AFSi, AFSrSiC and AFSrW powders were employed as insert layers to reactive diffusion bond  $SiC_p/6063$  MMC. The results show that  $SiC_p/6063$  MMC joints bonded by the insert layer of the mixed AFSi powder have a dense joining layer with a typical hypoeutectic microstructure. Using mixed AFSrSiC powder as insert layer,  $SiC_p/6063$  MMC can be reactive diffusion bonded by a composite joint. Because of the SiC segregations, however, there are a number of porous zones in the joining layer, which results in the low shear strength of the joints, even lower than that of joints reactive diffusion bonded by the insert layer of mixed AFSi powder. The W added into the insert layer of AFSrW nearly all reacts with Al to form intermetallic WAl<sub>12</sub> during bonding. The reaction between the W and Al facilitates to form a dense joint of high quality, and the formed intermetallic WAl<sub>12</sub> has a reinforcing effect on the joints, which lead to the high shear strength of the joints. In general, under the condition of fixed bonding time (temperature), the shear strengths of the joints increase as the bonding temperature (time) increases, but tend to a maximum at bonding temperature of 600  $^{\circ}$ C(time 90 min).

**Key words:** reactive diffusion bonding; insert powder layer; SiC<sub>p</sub>/Al MMCs **CLC number:** TG 456.9 **Document code:** A

## 1 INTRODUCTION

SiC<sub>p</sub> reinforced aluminium metal matrix composites (SiC<sub>p</sub>/Al MMCs) have a unique combination of mechanical and physical properties, such as high specific strength and specific modulus of elasticity, low thermal expansion coefficient and good wear resistance, being widely used in aerospace engineering, automotive industry, electronic packaging, medical appliances, etc. As is well known, joining is an indispensable processing for industrial applications of any material. Up to now, the majority of joining processes including fusion welding<sup>[1-8]</sup>, diffusion bonding<sup>[9-11]</sup> and brazing<sup>[12, 13]</sup> have been investigated to join SiC<sub>p</sub>/AlMMCs. Because of the specific characteristics in composition and microstructure, however, SiC<sub>p</sub>/Al MMCs display a bad join-ability. In fusion welding (TIG, MIG, EBW, LBW, etc), some weld defects, such as incomplete backfill, slag inclusions, blow holes and SiC segregation are liable to form in welded joints. Moreover, serious reaction between Al matrix and SiC particles will occur in the molten pool<sup>[1-6, 14]</sup>. Diffusion bonding need not melt the materials to be bonded during bonding, which should be an effective joining process for the heterogeneous composite materials, especially the ceramic particle reinforced metal matrix composites like the SiC<sub>p</sub>/Al MMCs. Unfortunately, the stable aluminium oxide film and the exposed SiC particles on the surface of the composites hinder atom diffusion and interfacial bonding during diffusion bonding. The direct solid diffusion bonding of the  $SiC_p/Al\ M\ M\ Cs$  is verified to be difficult. As for the brazing of  $SiC_p/Al\ M\ M\ Cs$ , a fatal weakness is the low strength of the brazed joints.

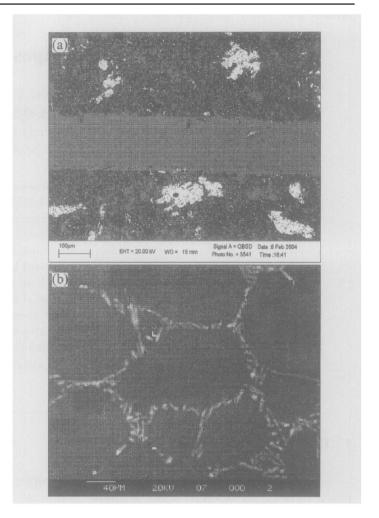
An effective method for joining of SiC<sub>p</sub>/Al MMCs is the process called as reactive diffusion bonding (RDB) or reactive brazing (RB), which is also classified as transient liquid phase diffusion bonding(TLP) by some investigations [15, 16]. Until the present, however, only the metal insert layers in the shape of foil, such as Cu foil, Ag foil, have been investigated to reactive diffusion bond the SiC<sub>p</sub>/Al MMCs<sup>[15]</sup>. Generally, there is a zone without composite in the joints of RDB by metal insert layers in the shape of foil, which obviously differs from the bonded composites in microstructure and mechanical properties. In addition, the foil metal insert layers have limitations on the structures to be bonded, being only suitable to bonding some simple structures. In order to explore a possible RDB process to surmount the limitations of the existent RDB process by foil metal insert layers on the structures to be bonded, and bond SiC<sub>p</sub>/Al MMCs by a joint with the mechanical properties, even with the composite microstructure similar to the bonded materials, in this investigation, mixed AFSi, AFSiFSiC and AFSiW powders are employed to replace foil metals as insert layers for reactive diffusion bonding of SiC<sub>p</sub>/Al MMCs, in which SiC and W powders are added in the insert layers as ceramic reinforcing phase and metal reinforcing phase respectively to obtain composite joints. Considering the bad wettability of SiC, W is investigated as reinforcing phase to add into the insert layer.

#### 2 EXPERIMENTAL

The composite material to be bonded in this investigation was 15% SiC<sub>p</sub> (volume fraction, %) reinforced 6063 aluminium alloy matrix composite (SiC<sub>p</sub>/6063 MMC), which was cut into samples of  $15 \text{ mm} \times 10 \text{ mm} \times 5 \text{ mm}$ . The particle sizes of the Al and Si powders as the reactive constituents, and the SiC and W powders as reinforcing phases of the joining layer were  $< 74 \,\mu m$ ,  $< 45 \,\mu m$ ,  $5 \,\mu m$  and 3-5 μm, respectively. The Al, Si, SiC and W powders were mixed with ethanol to prepare slurries of 87.4% Al + 12.6% Si (mass fraction), (87.4% Al+ 12.6% Si) + 10% SiC(volume fraction) and (87.4% Al+ 12.6% Si) + 10% W (volume fraction), respectively. The insert layers for bonding were prepared by coating the slurry on surfaces of the SiC<sub>p</sub>/6063 MMC samples to be bonded. The reactive diffusion bonding was performed at 580 -605 °C for 15 - 120 min under conditions of a pressure of  $3 \times 10^{-3}$  MPa, a vacuum of  $3.8 \times 10^{-3}$  Pa and heating rate of 10 °C/min. The X-ray diffraction(XRD) investigation was carried out using a Rigaku Rotaflex D/max-rb diffractometer. Microstructural observation for the joining layers was performed with a LEO-1450 scanning electron microscope.

## 3 RESULTS AND DISCUSSION

Fig. 1 shows the SEM micrographs (backscattered electron images) of a typical SiC<sub>p</sub>/6063 MMC joint reactive diffusion bonded by insert layer of the mixed AFSi powder. It is clear that a dense joint is formed by the eutectic reaction of Al and Si during bonding, and the interfaces between the bonded materials and the joining layer have a good bond. The joining layer is possessed of a typical hypoeutectic microstructure, which indicates that besides the Al added as the reactive constituents of the insert layer, some Al from the bonded composite dissolve into the joining layer. Fig. 2 shows the back-scattered SEM micrographs of a typical reactive diffusion bonded SiC<sub>p</sub>/6063 MMC joint by insert layer of the mixed AFSiSiC powder. The low magnification view (Fig. 2(a)) shows that the mixed AFSiSiC powder has reacted to



**Fig. 1** SEM micrographs of typical SiC<sub>p</sub>/6063MMC joint reactive diffusion bonded by insert layer of mixed AFSi powder

- (a) -Low magnification view;
- (b) —High magnification view

form a composite joint. Within the joining layer, however, there are a number of porous zones, which are demonstrated to result from the SiC segregations, as shown in the high magnification view of Fig. 2(b). The bad wettability of SiC for liquid aluminium base alloys is considered to be responsible for the SiC segregations. In fact, the bad wettability of SiC has been one of the problems for preparation of the SiC<sub>p</sub> reinforced aluminium metal matrix composites. The back-scattered SEM images of a typical SiC<sub>p</sub>/6063MMC joint reactive diffusion bonded by the mixed AFSFW powder as insert layer are shown in Figs. 3(a) and (b). It is interesting that the addition of W as reinforcing phase in the insert layer only facilitates to form a dense joint of high quality. Fig. 4 shows the X-ray diffraction pattern of the joining layer using mixed Al-Si-W powder as insert layer, by which only little pure W phase is found in the joining layer. The X-ray diffraction pattern and electron probe microanalyses as shown in Table 1 indicate that although W is attempted to add as metal reinforcing particles of joining layer into the insert layer, nearly all the

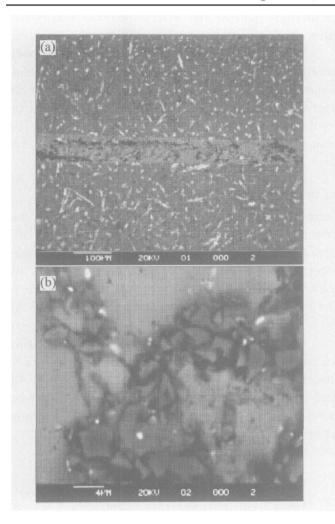


Fig. 2 SEM micrographs of typical SiC<sub>p</sub>/6063MMC joint reactive diffusion bonded by insert layer of mixed Al-Si-SiC powder

- (a) —Low magnification view;
- (b) -High magnification view

**Table 1** EPM A composition of characteristic zones in Fig. 3(b) (mass fraction, %)

Element	Zone A	Zone B
Al	59. 23	78.35
Si	1.53	21.65
W	39. 25	-

W in the insert layer reacts with Al to form intermetallic  $WAl_{12}$  (labeled A in Fig. 3 (b)) during bonding. The reaction between W and Al seems to be favorable for forming a dense joint.

The effects of bonding parameters (bonding temperature and time) on the shear strengths of the  $SiC_P/6063M\,M\,C$  joints reactive diffusion bonded by insert layers of the mixed AFSi, AFSiSiC and AFSiW powders are shown in Fig. 5. It is obvious that the joints bonded by the mixed AFSiW powder as insert layer present the highest shear strength reaching 72. 0 MPa. Evidently, the formation of the intermetallic WAl12 has not any detrimental effect on the joint shear strength, but

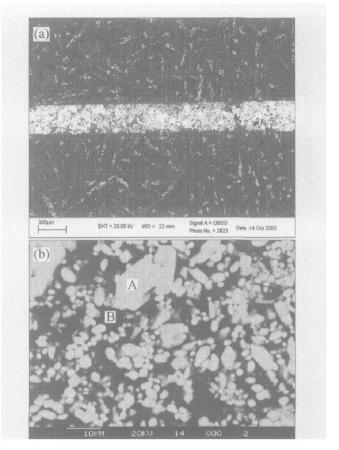
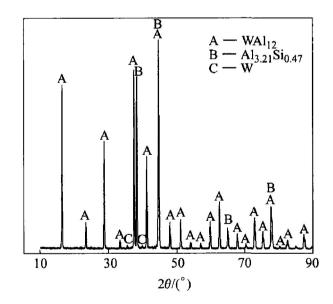


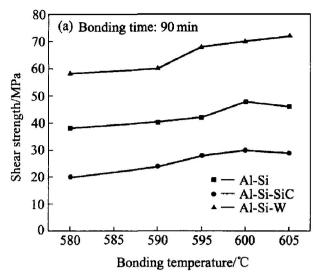
Fig. 3 SEM micrographs of typical SiC<sub>p</sub>/6063MMC joint reactive diffusion bonded by insert layer of mixed AlSiW powder

- (a) -Low magnification view;
- (b) —High magnification view



**Fig. 4** XRD pattern of joining layer by mixed AFSrW powder as insert layer

rather reinforces the joints. The W added into the insert layer still plays the role of reinforcing agent as designed. In the same figure, the joints reactive diffusion bonded by insert layer of the mixed AFSr SiC powder are shown to have a bad shear strength, even lower than that of joints reactive



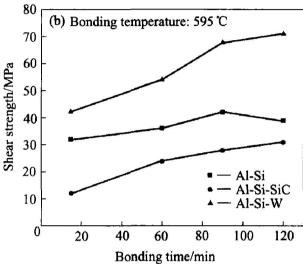


Fig. 5 Shear strengths of joints reactive diffusion bonded by insert layers of mixed AFSi, AFSiSiC and AFSiW powders vs bonding parameters

diffusion bonded by the insert layer of the mixed AFSi powder, which should be caused by the segregation of SiC particles and formation of the porous zones in joining layer. In the main, under the condition of fixed bonding time, the shear strengths of the joints by insert layers of the mixed AFSi, AFSiC and AFSi W powders increase as the bonding temperature rises, but tend to maxima at bonding temperature of 600 °C. Conversely, under the condition of fixed bonding temperature, all the shear strengths of the joints increase as the bonding time increases, and tend to a maximum at bonding time 90 min.

#### 4 CONCLUSIONS

1) Mixed Al-Si powder can be used as insert layer to reactive diffusion bond SiC<sub>p</sub>/Al MMCs. The SiC<sub>p</sub>/6063 MMC joints bonded by insert layer of the mixed Al-Si powder have a dense joining layer of high quality and a hypoeutectic microstruc-

ture.

- 2) Using mixed AFSiSiC powder as insert layer,  $SiC_p/6063$  MMC can be reactive diffusion bonded by a composite joint. However, the SiC segregation results in the low shear strength of the joints, even lower than that of joints reactive diffusion bonded by insert layer of the mixed AFSi powder.
- 3) W added into insert layer of the mixed AFSrW powder nearly all reacts with Al to form intermetallic WAl $_{12}$  during bonding. The reaction between the W and Al facilitates the formation of a dense joint of high quality. In addition, the formed intermetallic WAl $_{12}$  has a reinforcing effect on the joints, which leads to the high shear strength of the joints bonded by insert layer of the mixed AFSrW powder.
- 4) Under the condition of fixed bonding time (temperature), the shear strengths of the joints by insert layers of both the mixed AFSi, AFSrSiC and AFSrW powders increase as the bonding temperature (time) increases, but tend to a maximum at bonding temperature 600 °C(time 90 min).

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