

Electrochemical properties of $\text{CeMg}_{11}\text{Ni} + x\% \text{ Ni}$ composites ($x = 0, 50, 100$ and 200) prepared by ball-milling^①

WANG Li(王丽), WANG Xin-hua(王新华),
CHEN Li-xin(陈立新), CHEN Chang-pin(陈长聘)

(Department of Materials Science and Engineering, Zhejiang University,
Hangzhou 310027, China)

Abstract: The electrochemical properties of the as-cast $\text{CeMg}_{11}\text{Ni}$ and ball-milled $\text{CeMg}_{11}\text{Ni} + x\% \text{ Ni}$ ($x = 0, 50, 100$ and 200 , mass fraction) composites were investigated. The results show that homogeneous amorphous phase of $\text{CeMg}_{11}\text{Ni} + x\% \text{ Ni}$ composite can be obtained by ball-milling, and discharge capacity of the ball-milled $\text{CeMg}_{11}\text{Ni} + x\% \text{ Ni}$ composites differs greatly depending on the amount of Ni introduced during milling. The $\text{CeMg}_{11}\text{Ni} + 200\%$ Ni composite after 90 h ball-milling was found to exhibit a large discharge capacity of about 1012 mAh/g at 303 K , and it also shows better charge-discharge cycling stability than those with lower Ni content. This remarkable improvement in electrochemical properties of the ball-milled composites seems to be attributed to the formation of an amorphous composite as well as the improvement of the surface state of the ball-milled particles.

Key words: hydrogen storage alloy; $\text{CeMg}_{11}\text{Ni}$; amorphous phase; electrochemical properties

CLC number: TG 139

Document code: A

1 INTRODUCTION

Magnesium and magnesium-based alloys are promising hydrogen storage materials because of their absorbability of hydrogen in large quantities, low specific gravity, rich mineral resources, low material cost and so on. Nevertheless, their hydrides are too stable to be used at room temperature^[1]. It seems impossible for application of crystalline Mg-based alloys in nickel-hydrogen batteries.

It is well known that amorphous alloys have many advantageous properties over crystalline ones. However, amorphous Mg-based hydrogen storage alloys have not attracted much attention till the end of 1980s because they cannot be prepared by the conventionally used rapid solidification method. In early 1990s, Lei et al^[2, 3] reported that amorphous Mg-Ni alloys prepared by mechanical alloying of Mg and nickel powder. Since then many researchers have directed their work to Mg-Ni amorphous alloys^[4, 5]. Kohno et al^[6, 7] found that by mechanical grinding of Mg_2Ni with Ni, a discharge capacity of about 750 mAh per gram of Mg_2Ni (485 mAh per gram of $\text{Mg}_2\text{Ni} + 100\%$ Ni) had been reached. Nohara et al^[8, 9] reported the enhanced electrochemical characteristics of a nanocrystalline Mg_2Ni and a homogeneous amorphous alloy prepared by ball-milling of Mg_2Ni without or

with Ni, and the latter exhibited a maximum discharge capacity of about 870 mAh per gram of Mg_2Ni (512 mAh per gram of $\text{Mg}_2\text{Ni} + 70\%$ Ni) at 303 K . Iwakura et al^[10] reported an even higher discharge capacity of about 1082 mAh per gram of Mg_2Ni (636 mAh per gram of $\text{Mg}_2\text{Ni} + 70\%$ Ni), which exceeded the theoretically calculated value of 999 mAh per gram of Mg_2Ni on the basis of Mg_2NiH_4 for crystalline Mg_2Ni . These improvements in the characteristics of Mg_2Ni alloy are mainly caused by the appearance of a nanocrystalline or amorphous structure.

The hydrogen storage capacity of Ln-Mg ($\text{Ln} = \text{La, Ce or mischmetal}$) series alloys such as $\text{La}_2\text{Mg}_{17}$ and CeMg_{12} reaches 6.0% , much higher than that of Mg_2Ni alloy^[11, 12]. However, the electrochemical properties of amorphous A_2B_{17} and AB_{12} type Ln-Mg alloys are seldom reported. In our previous work^[13], it was found that the amorphous $\text{La}_{1.8}\text{Ca}_{0.2}\text{Mg}_{14}\text{Ni}_{13} + 100\%$ Ni composite after 50 h ball-milling exhibits a large discharge capacity of 1004 mAh per gram of $\text{La}_{1.8}\text{Ca}_{0.2}\text{Mg}_{14}\text{Ni}_{13}$ at 298 K . In the present work, the electrochemical properties of $\text{CeMg}_{11}\text{Ni} + x\% \text{ Ni}$ ($x = 0, 50, 100, 200$) composites prepared by ball-milling method were studied in comparison with the as-cast $\text{CeMg}_{11}\text{Ni}$ alloy. The emphasis was placed on the

① **Foundation item:** Project (TG2000026406) supported by the National Basic Research Development Program of China; Project (50471042) supported by the National Natural Science Foundation of China

Received date: 2004-11-15; **Accepted date:** 2005-01-18

Correspondence: WANG Li, PhD; Tel: +86-571-87951152; E-mail: tigerwl29@yahoo.com.cn

influence of the amount of Ni on the microstructures and on the electrochemical capacities of the ball-milled composites.

2 EXPERIMENTAL

CeMg₁₁Ni alloy was first prepared in an induction furnace and this alloy was mechanically pulverized to particles below 49 μm . The CeMg₁₁Ni alloy powder thus prepared was mixed with Ni powder in mass ratios of 1: 0, 1: 0.5, 1: 1 and 1: 2 (total mass of 1.5 g), respectively, followed by ball-milling under argon atmosphere for 90 h at a rate of 350 r/min. The resulting powder will be designated hereafter as CeMg₁₁Ni+ x% Ni ($x = 0, 50, 100, 200$) composites.

Each sample powder was mixed with Ni powder again in mass ratio of 1: 4, and 0.5 g mixture was pressed under a pressure of 12 MPa to form a pellet with diameter of 10 mm. Electrochemical measurements were performed in a three-electrode system and a 6 mol/L KOH aqueous solution was used as electrolyte. A nickel electrode ($\text{Ni(OH)}_2/\text{NiOOH}$) was used as the counter electrode and a mercury (II) oxide electrode (Hg/HgO , 6 mol/L KOH) was used as the reference electrode. The discharge capacity and the cycle life of the test electrodes were determined by the galvanostatic method. The test electrodes were charged at 100 mA/g and discharged at 60 mA/g to the cut-off potential of -0.55 V (vs Hg/HgO). After each charging, there was a 10 min break. The electrochemical tests were all carried out at 303 K. The discharge capacities of these sample alloys were calculated and expressed per gram of CeMg₁₁Ni.

The X-ray diffraction study was carried out on a Rikagu D/Max PC2500 X-ray diffractometer with Cu K α radiation. The surface morphology of the ball-milled alloy powder was examined in a scanning electron microscope (SEM).

3 RESULTS AND DISCUSSION

3.1 Microstructures

The X-ray diffraction patterns of the as-cast CeMg₁₁Ni and ball-milled CeMg₁₁Ni+ x% Ni ($x = 0, 50, 100, 200$) composites are presented in Fig. 1. As can be seen from Fig. 1, initially the as-cast CeMg₁₁Ni alloy mainly contains CeMg₁₂ phase, additionally, little amount of Mg₂Ni and CeO₂ were also detected. The CeO₂ may be due to the oxidation of the alloy by the oxygen in the air. After ball-milling without Ni addition, the diffraction peaks of CeMg₁₂ apparently broaden and merge, which indicates that grain size is reduced and a nanocrystalline structure may be formed. For

the ball-milled CeMg₁₁Ni+ x% Ni composites, in case of $x = 50$, besides the broadened peaks of CeMg₁₂ phase, some characteristic diffraction peaks of metallic Ni (at positions $2\theta = 44.5^\circ, 51.8^\circ$ and 76.5°) appear. However, as the value of x increases, the peaks of crystalline CeMg₁₂ and Ni phases all weaken. In the case of the ball-milled CeMg₁₁Ni+ 100% Ni composite, a small broadened Ni peak is found coexisting with the broad hump, which reveals that some nanocrystalline Ni is embedded in the amorphous matrix. But when x increases to 200, the crystalline diffraction peaks of CeMg₁₂ and Ni have disappeared completely and a single hump appears at 2θ angles of 40° – 42° , indicating that a homogeneous amorphous phase has been formed for this ball-milled composite.

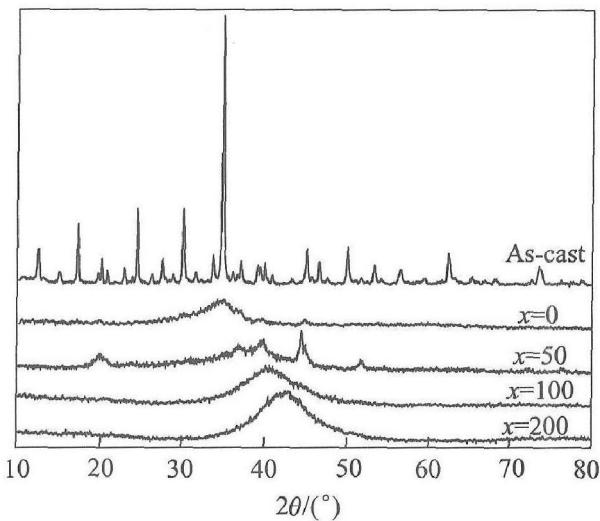


Fig. 1 XRD patterns of as-cast CeMg₁₁Ni and ball-milled CeMg₁₁Ni+ x% Ni ($x = 0, 50, 100, 200$) composite

Based on the above analysis, it is clear that Ni addition is very effective in enhancing the amorphorization of the CeMg₁₁Ni alloy and the amount of Ni added is the key factor influencing the amorphorization in the present case.

3.2 Electrochemical properties

The discharge curves of the as-cast CeMg₁₁Ni alloy and ball-milled CeMg₁₁Ni+ x% Ni ($x = 0, 50, 100, 200$) composites at their respective discharge capacity are shown in Fig. 2.

From Fig. 2, we can see that the obtained discharge capacities of CeMg₁₁Ni ball-milled with Ni are greater than those of the as-cast alloy and the ball-milled composite without Ni addition. It is known that the electrochemical hydriding and dehydriding procedures of hydrogen storage alloy electrode in an alkaline solution include at least two steps^[14]: electrochemical (charge transfer) step and diffusion step. The electrode reaction can be expressed as

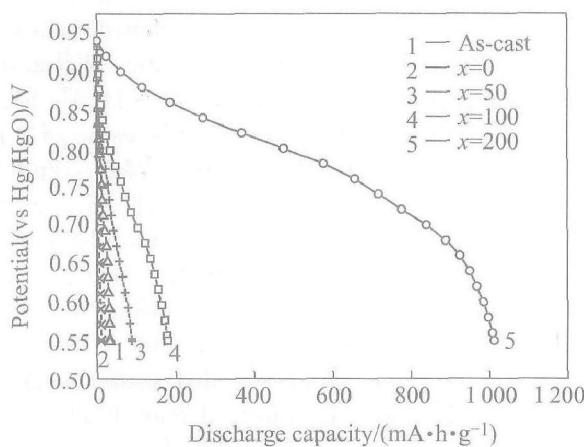
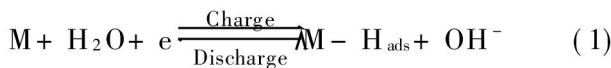


Fig. 2 Discharge curves of as-cast $\text{CeMg}_{11}\text{Ni}$ alloy and ball-milled $\text{CeMg}_{11}\text{Ni} + x\% \text{Ni}$ ($x = 0, 50, 100, 200$) composites at their respective maximum discharge capacity at 303 K



It can be seen that the performance of electrochemical hydriding and dehydriding reactions in an alkaline solution is determined by both the charge transfer reaction on the alloy/electrolyte interface (Eqn. (1)) and the rate of hydrogen diffusion within the bulk of the alloy (Eqn. (2)).

Nickel is well known to have a high electrocatalytic activity or a low overpotential for the hydrogen evolution reaction (HER) in alkaline solution.

The nickel particles inserted in the $\text{CeMg}_{11}\text{Ni}$ alloy are, therefore, believed to act as the electrocatalytic active sites for the HER so that they may reduce the charge transfer resistance, resulting in a significant increase of the electrochemical capacity. Fig. 3 shows the SEM images of the ball-milled $\text{CeMg}_{11}\text{Ni} + x\% \text{Ni}$ ($x = 0, 50, 100, 200$) composites. As shown in Fig. 3, with the increase of Ni amount, the particle size decreases to different extent. The decrease of the particle size and the augmentation of the density of defects may improve the diffusion of hydrogen in the alloy, which is also believed to be beneficial for improving hydriding/dehydriding reactions. Thus the ball-milled primary $\text{CeMg}_{11}\text{Ni}$ alloy with nickel powder is not simply a mixture of two components, but a new composite system with high reactivity due to the inlaid electrocatalytic active sites, the large interface, the small interface, the small crystallite size and the presence of defects. And all the above factors lead to the higher discharge capacities of the composites ball-milled with Ni.

From Fig. 2 it can also be clearly seen that the discharge capacity of the ball-milled $\text{CeMg}_{11}\text{Ni}$ with Ni differs greatly depending on the amount of Ni introduced during milling. The discharge capacities of the ball-milled $\text{CeMg}_{11}\text{Ni} + 50\%$ Ni and $\text{CeMg}_{11}\text{Ni} + 100\%$ Ni composites are only 90 and 180 mA·h/g, respectively. But in the case of the ball-milled $\text{CeMg}_{11}\text{Ni} + 200\%$ Ni composite with a homogeneous amorphous structure, a plateau of the potential based on the oxidation of desorbed hydro-

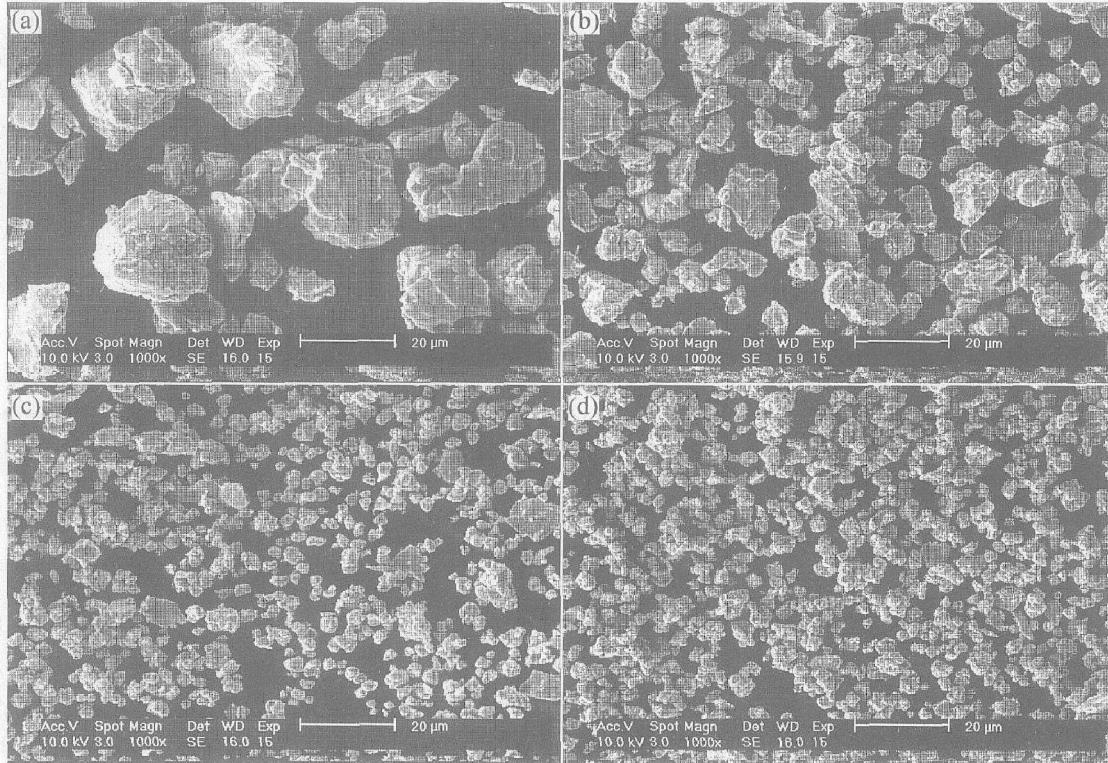


Fig. 3 SEM images of ball-milled $\text{CeMg}_{11}\text{Ni} + x\% \text{Ni}$ ($x = 0, 50, 100, 200$) composites
(a) $x = 0$; (b) $x = 50$; (c) $x = 100$; (d) $x = 200$

gen was observed at more negative potential than that for other composites, and an extremely high discharge capacity was exhibited, about 1 012 mA·h per gram of CeMg₁₁Ni (337 mA·h per gram of CeMg₁₁Ni+ 200% Ni). The marked improvement in discharge characteristics of the CeMg₁₁Ni alloy ball-milled with 200% Ni seems to be partly ascribed to the formation of homogeneous amorphous region which can have a higher equilibrium hydrogen pressure and make the desorption of hydrogen much easier. In other words, the discharge capacity depends to a great degree on the amorphorization degree of the composite alloy. From Fig. 1 we can see that the amorphorization degree of the composite alloy increases with the increasing amount of Ni, and thus leads to the result that the discharge capacity increases with the increasing Ni amount during ball-milling. On the other hand, from Fig. 4 we can see that the particle size of the ball-milled CeMg₁₁Ni+ x% Ni (x = 50, 100, 200) composites decreases with the increasing Ni amount, especially in the case of the ball-milled CeMg₁₁Ni+ 200% Ni composite, the particle size decreases a lot. As the particle size decreases, the discharge capacity increases due to the increase in effective surface area for hydrogen electrode reaction and shortened hydrogen diffusion length. So the discharge capacity of the ball-milled CeMg₁₁Ni+ 200% Ni composite exhibits a larger increase compared with the others. These results clarify that mechanical grinding with proper amount of Ni powder is an effective way to improve the charge-discharge capability of the negative electrode containing Mg-based alloy.

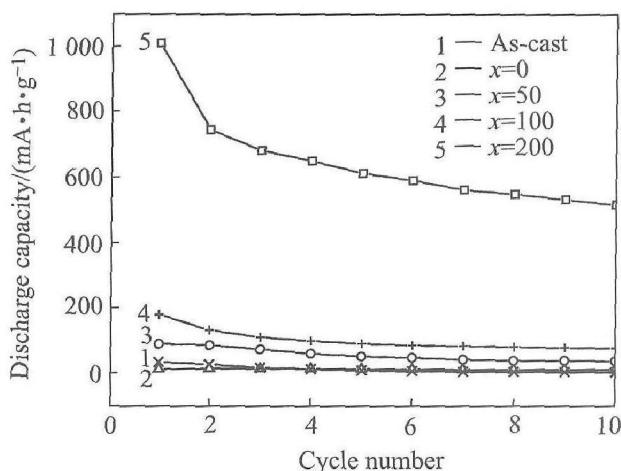


Fig. 4 Discharge capacities as function of cycle number for as-cast CeMg₁₁Ni alloy and ball-milled CeMg₁₁Ni+ x% Ni (x = 0, 50, 100, 200) composites at 303 K

Fig. 4 shows the specific discharge capacities as function of cycle number for the ball-milled CeMg₁₁Ni+ x% Ni (x = 0, 50, 100, 200) com-

posites at 303 K. And Table 1 lists the maximum discharge capacity and cycling retention rate of the composites after 10 cycles.

Table 1 Maximum discharge capacity(mA·h/g) and cycling retention rate(%) of ball-milled CeMg₁₁Ni+ x% Ni(x = 0, 50, 100, 200) composites after 10 cycles

x	$C_m / (\text{mA} \cdot \text{h} \cdot \text{g}^{-1})$	$C_{m+10} / (\text{mA} \cdot \text{h} \cdot \text{g}^{-1})$	Retention rate/ %
0	12.4	9.3	75.0
50	89.8	35.5	39.5
100	180.5	75.7	41.9
200	1 012.1	515.2	50.9

For the ball-milled CeMg₁₁Ni+ 100% Ni composite the discharge capacity decreases to 41.9% of its original one after 10 cycles. While the composite with x = 200 can maintain 515.2 mA·h/g and 50.9% of its initial discharge capacity. This means that compared with the ball-milled CeMg₁₁Ni+ 100% Ni composite, the ball-milled CeMg₁₁Ni+ 200% Ni composite not only has a higher discharge capacity, but also its cycling stability is improved. This may be attributed to the fact that the higher Ni content reduces the contact between Mg and the KOH solution, and thus can enhance the stability of the composite. It is ever reported^[15] that nanocrystalline Mg₂Ni alloy lost 80% of its maximum discharge capacity within 10 cycles. Compared with the rapid capacity degradation of Mg-Ni type alloys, the cycle life of the samples is improved. The slower deterioration of the cycle stability may be explained by the existence of Ce, which forms a passive oxide layer on the particle surface reducing the contact of Mg with alkaline solution, thus prolonging the cycle lifetime of the Ce-Mg system alloys.

4 CONCLUSIONS

Mechanical grinding with nickel powder is an effective method of improving the electrode properties of Mg-based alloys because of the changed amorphous structure. The amount of Ni added has an important influence on the amorphorization degree in certain duration ball-milling. After 90 h of ball-milling, a homogenous amorphous CeMg₁₁Ni+ 200% Ni composite is formed, and its discharge capacity reaches 1 012 mA·h per gram of CeMg₁₁Ni. Complete amorphorization of the composites, which in turn is influenced by the amount of Ni added, turns out to be the main factor controlling the electrochemical capacity. The Ni addition also changes the surface state, and enhances

the charge transfer reaction and hydrogen diffusion at the surface, thus accelerating the electrochemical reaction. More Ni addition improves the charge-discharge cycling stability of the ball-milled composite due to the reduced contact between Mg and the KOH solution.

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(Edited by LONG Huai-zhong)