

## Electrochemical behavior and polishing properties of silicon wafer in alkaline slurry with abrasive CeO<sub>2</sub>

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**Abstract:** The electrochemical behavior of silicon wafer in alkaline slurry with nano-sized CeO<sub>2</sub> abrasive was investigated. The variations of corrosion potential ( $\varphi_{\text{corr}}$ ) and corrosion current density ( $J_{\text{corr}}$ ) of the P-type (100) silicon wafer with the slurry pH value and the concentration of abrasive CeO<sub>2</sub> were studied by polarization curve technologies. The dependence of the polishing rate on the pH and the concentration of CeO<sub>2</sub> in slurries during chemical mechanical polishing(CMP) were also studied. It is discovered that there is a large change of  $\varphi_{\text{corr}}$  and  $J_{\text{corr}}$  when slurry pH is altered and the  $J_{\text{corr}}$  reaches the maximum (1.306  $\mu\text{A}/\text{cm}^2$ ) at pH 10.5 when the material removal rate(MRR) comes to the fastest value. The  $J_{\text{corr}}$  increases gradually from 0.994  $\mu\text{A}/\text{cm}^2$  with 1% CeO<sub>2</sub> to 1.304  $\mu\text{A}/\text{cm}^2$  with 3% CeO<sub>2</sub> and reaches a plateau with the further increase of CeO<sub>2</sub> concentration. There is a considerable MRR in the slurry with 3% CeO<sub>2</sub> at pH 10.5. The coherence between  $J_{\text{corr}}$  and MRR elucidates that the research on the electrochemical behavior of silicon wafers in the alkaline slurry could offer theoretic guidance on silicon polishing rate and ensure to adjust optimal components of slurry.

**Key words:** Chemical mechanical polishing(CMP); material removal rate(MRR); electrochemical characteristics; slurry; abrasive CeO<sub>2</sub>

### 1 Introduction

Chemical mechanical polishing(CMP) was firstly put forward in 1991 by IBM and replaced the traditional method gradually, such as single chemical polishing and single mechanical polishing. CMP not only made a better surface, but also provided higher polishing flatness and was commonly recognized as the only and best method of achieving global planarization[1–5].

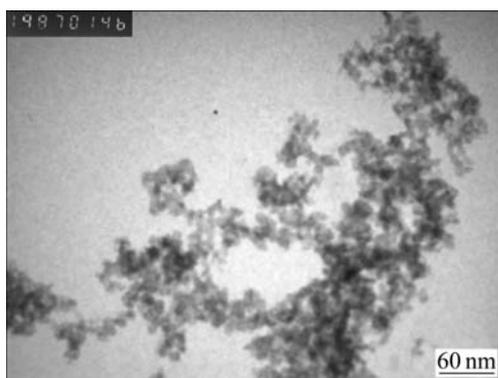
Colloid SiO<sub>2</sub> aqueous suspension was the most widely used slurry in semiconductor industry, but the polishing rate of silica colloid was lower compared with other polishing oxides. Abrasive CeO<sub>2</sub> polishing had high rate and it was widely adopted in the glass polishing, but its usage in CMP of silicon wafer was little found in literatures and the researches were few[6–9]. So in this work the polishing properties of silicon wafer in slurry with abrasive CeO<sub>2</sub> are investigated and the

research on the electrochemical behavior of silicon wafers in the slurry, which could offer theoretic guidance on the silicon corrosion, was conducted as well[10–11]. Through these studies we could realize the factors that influence corrosion rates of silicon wafers more clearly, and we could quantitatively elucidate how to control the polishing parameters, which was very important to improve polishing quality.

### 2 Experimental

#### 2.1 Chemicals and samples

Chemicals included nano-sized CeO<sub>2</sub> abrasive (average diameter 20 nm). The synthesis method of nano-sized CeO<sub>2</sub> was described previously[12] and the TEM photograph of nano-sized CeO<sub>2</sub> powders is shown in Fig.1. Surfactant (NaPO<sub>3</sub>)<sub>6</sub>,  $\beta$ -Hydroxyethyl Diamine ( $\geq 99\%$ ), CH<sub>3</sub>COOH (99.5%), HF, NH<sub>4</sub>F and deionised water were utilized. All of the chemicals were



**Fig.1** TEM photograph of nano-sized  $\text{CeO}_2$  powders

in analytically pure grade. The alkaline slurry was obtained by the following steps: Firstly, confect 225 mg/L solution of  $(\text{NaPO}_3)_6$  (When  $\text{CeO}_2$  suspension contained 225 mg/L surfactant  $(\text{NaPO}_3)_6$ , the  $\text{CeO}_2$  particles came to the best dispersion in solution[13]); Secondly, add certain quality of abrasive  $\text{CeO}_2$  to the former solution and then disperse the slurry by ultrasonic wave (frequency 100 kHz) for 20 min; Finally, adjust the pH of slurry with  $\beta$ -Hydroxyethyl Diamine or  $\text{CH}_3\text{COOH}$ .

In the experiment, samples were czochralski grown, boron-doped P-Si (100) wafer ( $1\text{--}5 \Omega\cdot\text{cm}$ , orientation tolerance  $\pm 0.5^\circ$ ). The silicon working electrode prepared for electrochemical experiments was mounted in a cylindrical of Teflon holder and the exterior surface was limited with an "O"-ring with diameter of 1.33 cm.

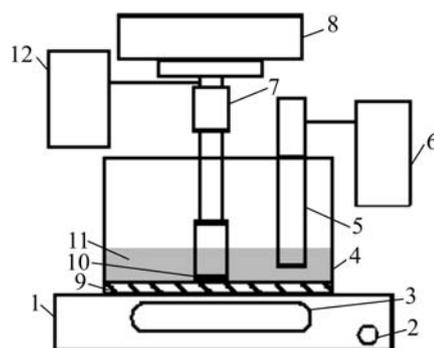
## 2.2 Electrochemical measurements

For electrochemical measurements, native oxide needed to be removed before each measurement by soaking the wafer in 1 mol/L HF+2 mol/L  $\text{NH}_4\text{F}$  for 1 min followed by rinsing with deionised water. The electrochemical experiments were carried out with the silicon working electrode, a platinum counter electrode and an Ag/AgCl reference electrode with a Luggin probe. The static electrochemical DC polarization measurements were conducted by a Potentiostat/Galvanostat of EG&G Model 273A, and the corrosion software of EG&G Model 352 was adopted for electrochemical calculations. During the potentiodynamic scan, the working electrode potential varied with a scan rate of 1 mV/s from  $-0.6 \text{ V}$  to  $0.4 \text{ V}$  for measuring the corrosion current density and potential.

## 2.3 MRR of CMP measurements

The system of polishing experiment adopted is shown in Fig.2. Polishing time was 30 min; rotation rate was 200 r/min; imposed pressure was  $0.10 \text{ kg/cm}^2$  and temperature of the slurry was  $(30 \pm 1) ^\circ\text{C}$ .

The material removal rate(MRR) was determined



**Fig.2** Schematic diagram of polishing experiment system: 1 Pressure sensor; 2 Button of elevator; 3 Display of pressure sensor; 4 Cell; 5 pH-meter; 6 Display of pH-meter; 7 Monitor of rotation rate; 8 Shelf; 9 Polishing pad; 10 Silicon wafer; 11 Slurry; 12 Rotation motor

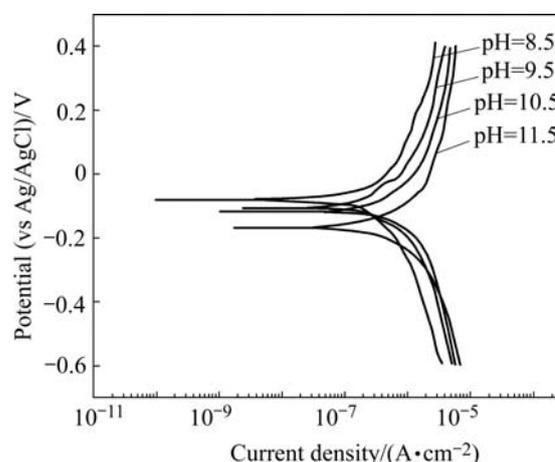
by measuring the thickness of polished silicon as a function of polishing time.

## 3 Results and discussion

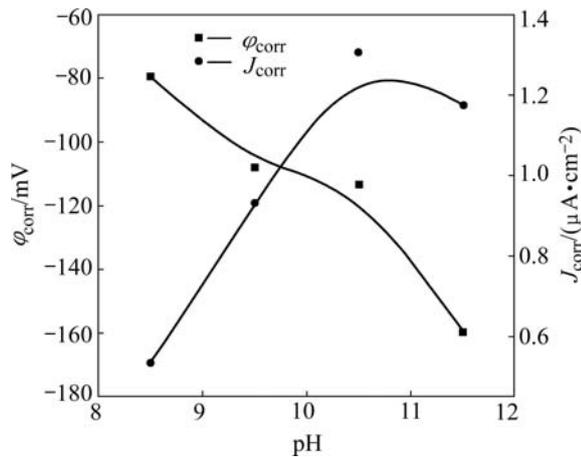
### 3.1 Dependence of polarization curves of P-Si (100) on pH value

Fig.3 shows the potentiodynamic polarization curves for P-Si (100) silicon tested in the slurries with 3% (mass fraction)  $\text{CeO}_2$  at various pH values. The corrosion current densities and the potentials of Fig.3 determined by the corrosion software of EG&G Model 352 are plotted in Fig.4. As can be seen from Fig.4, the corrosion potential decreased firstly with the increase of pH, and then increased to the maximum of  $1.306 \mu\text{A/cm}^2$  at pH of 10.5; with the further increase of pH, the current density decreased to  $1.175 \mu\text{A/cm}^2$  at pH of 11.5. This implied that the dissolution rate came to the fastest value in the slurry with pH 10.5.

The etching process of silicon was described as

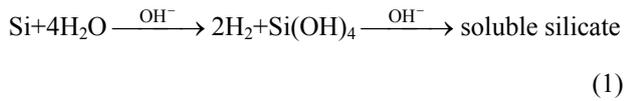


**Fig.3** Potentiodynamic polarization curves of P-Si (100) in slurries with 3%  $\text{CeO}_2$  at various pH values



**Fig.4** Variation of corrosion potential  $\phi_{\text{corr}}$  and corrosion current density  $J_{\text{corr}}$  of P-Si (100) in slurries with 3%  $\text{CeO}_2$  as a function of pH

follows: two hydrogen molecules were released for each silicon atom dissolved and  $\text{Si}(\text{OH})_4$  was regarded the primary reaction product[14–15]. The overall reaction was[16–17]



The process involved the hydroxide ion catalysed reaction of silicon and water to provide hydrogen and silicates. Namely, the dissolution rate was related to water and hydroxide ion concentration. GLEMBOCKI et al[18] proposed a model to explain the existence of dissolution rate peak based on the assumption that both free water and hydroxide ions were etching species. The reaction rate equation could be expressed as

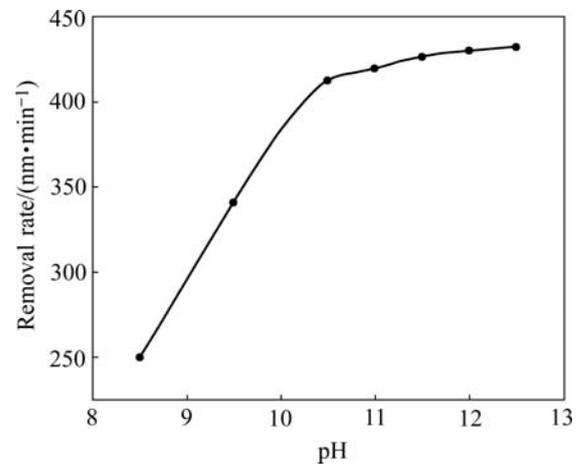
$$R = C[\text{H}_2\text{O}_{\text{free}}]^r [\text{OH}_{\text{free}}^-]^s \quad (2)$$

According to the model, water was composed of free water and bound water. Free water and hydroxide ions were the major particles that participated in the chemical reaction. As pH increased, the  $\text{OH}^-$  concentration increased, while  $\text{H}_2\text{O}_{\text{free}}$  concentration decreased. So these two competing effects made the peak in the corrosion rate.

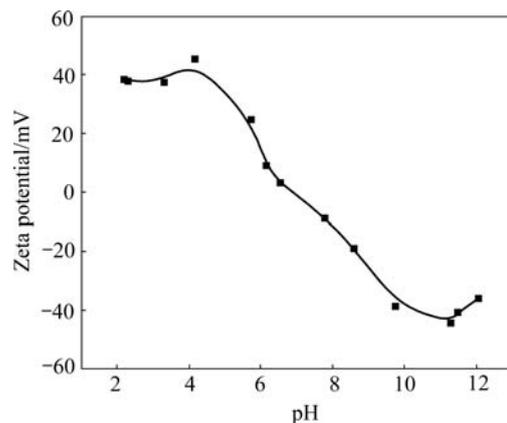
### 3.2 Dependence of CMP material removal rate on pH

As shown in Fig.5, a pronounced increase of MRR with the increase of pH was observed, and then MRR reached a plateau at pH 10.5 and finally kept approximately horizontal. The sharp increase of MRR could be ascribed to hydroxide ion concentration increase and resulted in corrosion rate enhancement as the foregoing analysis. On the other hand, pH had an

important influence on  $\text{CeO}_2$  particles dispersion in solution. Fig.6 shows the Zeta potential of particle surface at various pH values. A minimum negative Zeta potential around pH 10.5 indicated that there was a superior dispersion of abrasive  $\text{CeO}_2$  in alkaline solution with pH 10.5. Stable dispersion of abrasive  $\text{CeO}_2$  in slurry helped to improve material removal rate and polishing silicon surface quality. Subsequently, the plateau state in the removal rate was due to limited mechanical effect. As it is well known, chemical mechanical polishing consists of two aspects: chemical corrosion effect and mechanical abrasion effect. When the chemical corrosion effect surpasses the mechanical abrasion effect, MRR depends on the latter. Only under fit cooperation between them can it be expected to reach an optimal MRR level[19].



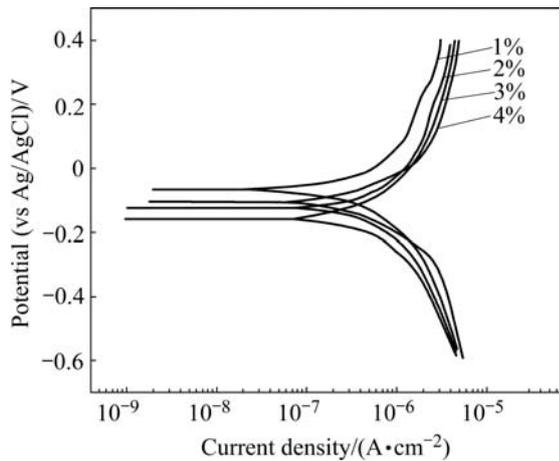
**Fig.5** Dependence of CMP material removal rate on pH



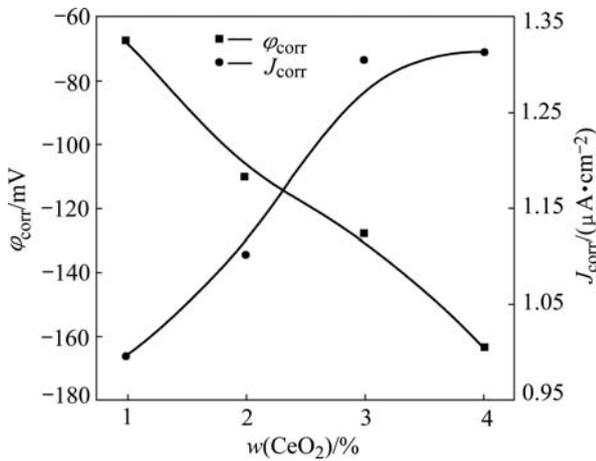
**Fig.6** Dependence of Zeta potential of  $\text{CeO}_2$  particle surface on pH

### 3.3 Dependence of polarization curves of P-Si (100) silicon on concentration of $\text{CeO}_2$

Fig.7 presents the potentiodynamic polarization curves for P-Si (100) in the slurries with different concentrations of abrasive  $\text{CeO}_2$  at pH 10.5. As can be seen from Fig.7, the shape of the polarization curves with different concentrations was very similar. From Fig.8,



**Fig.7** Potentiodynamic polarization curves of P-Si (100) in slurries with different concentrations of abrasive CeO<sub>2</sub> at pH 10.5



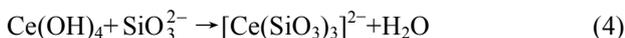
**Fig.8** Variation of corrosion potential and corrosion current density of P-Si (100) in slurries at pH 10.5 as function of CeO<sub>2</sub> abrasive concentration

the corrosion potential ranged from  $-67.8$  mV with 1% CeO<sub>2</sub> to  $-163.7$  mV with 4% CeO<sub>2</sub>, indicating concentration of CeO<sub>2</sub> had some influence on the film thickness. The corrosion current density increased gradually from  $0.994 \mu\text{A}/\text{cm}^2$  with 1% CeO<sub>2</sub> to  $1.304 \mu\text{A}/\text{cm}^2$  with 3% CeO<sub>2</sub>; then with the further increase of concentration, the current density leveled off to  $1.313 \mu\text{A}/\text{cm}^2$ .

As well known, amphoteric oxide CeO<sub>2</sub> would have a hydration in slurry:



Because of the complexation of CeO<sub>2</sub>, the corrosion product  $\text{SiO}_3^{2-}$  could be transformed into  $[\text{Ce}(\text{SiO}_3)_3]^{2-}$  and the equation could be written as

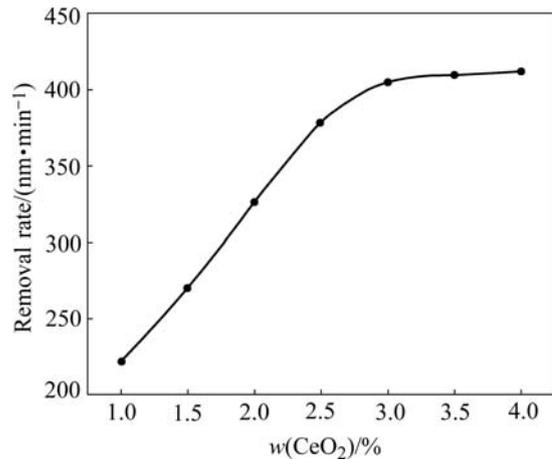


which resulted in accelerated removal of  $\text{SiO}_3^{2-}$  from

silicon surface and promoted corrosion rate and corrosion current density. When CeO<sub>2</sub> concentration reached 3%, because of sufficient complexation, the corrosion current density leveled off.

### 3.4 Dependence of CMP material removal rate on concentration of CeO<sub>2</sub>

The abrasive, during the polishing process, affected the mechanical abrasion of the corrosion layer. As shown in Fig.9, with increase of abrasive concentration, MRR rose from 225 nm/min with 1% CeO<sub>2</sub> to 406 nm/min with 3% CeO<sub>2</sub> and 412 nm/min with 4% CeO<sub>2</sub>. The functional relation of MRR of silicon in CMP process with the concentration of CeO<sub>2</sub> in slurries at pH 10.5 presented the same tendency as that of the corrosion current density with the concentration of CeO<sub>2</sub> indicated in Fig.8 under the same condition. This indicates that abrasive CeO<sub>2</sub> accelerates reaction product silicates departure from silicon plane by complexation of Ce(OH)<sub>4</sub>.



**Fig.9** Dependence of CMP material removal rate on concentration of CeO<sub>2</sub> in slurries at pH 10.5

## 4 Conclusions

1) The results of polarization curves reveal that pH of the slurry has a pronounced influence on the silicon wafer corrosion. The current density increases with the increase of pH and reaches the maximum ( $1.306 \mu\text{A}/\text{cm}^2$ ) at pH 10.5, then with the further increase of pH, the current density decreases to  $1.175 \mu\text{A}/\text{cm}^2$  at pH 11.5. This implies that the corrosion rate comes to the fastest value in the slurry at pH 10.5.

2) The corrosion current density increases gradually from  $0.994 \mu\text{A}/\text{cm}^2$  with 1% CeO<sub>2</sub> to  $1.304 \mu\text{A}/\text{cm}^2$  with 3% CeO<sub>2</sub>, and then with the further increase of concentration, the current density levels off. This implies that there is an optimal dissolution rate in the slurry with 3% CeO<sub>2</sub> at pH 10.5.

3) In the MRR of CMP experiment, a marked

increase of MRR with the increase of pH is observed and MRR reaches a plateau (412 nm/min) at pH 10.5. Dependence of MRR on concentration of CeO<sub>2</sub> is the same as that on pH and reaches considerable value of 406 nm/min in the slurry with 3% CeO<sub>2</sub>.

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