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# Synthesis of Li<sup>+</sup> adsorbent (H<sub>2</sub>TiO<sub>3</sub>) and its adsorption properties

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**Abstract:**  $H_2TiO_3$  was obtained from the acid-modified adsorbent precursor  $Li_2TiO_3$ , which was synthesized by a solid-phase reaction between  $TiO_2$  and  $Li_2CO_3$ . The extraction ratio of  $Li^+$  from  $Li_2TiO_3$  was 98.86%, almost with no  $Ti^{4+}$  extracted. The effects of lithium titanium ratio, calcining temperature and time were investigated on the synthesis of  $Li_2TiO_3$ .  $Li_2TiO_3$ ,  $H_2TiO_3$  and the adsorbed  $Li^+$  adsorbent were characterized by XRD and SEM. The lithium adsorption properties were investigated by the adsorption kinetics and adsorption isotherm. The results indicate that  $H_2TiO_3$  has an excellent adsorptive capacity for  $Li^+$ . Two simplified kinetic models including the pseudo-first-order and pseudo-second-order equations were selected to follow the adsorption processes. The rate constants of adsorption for these kinetic models were calculated. The results show that the adsorption process can be described by the pseudo-second-order equation, and the process is proved to be a chemical adsorption. The adsorption process that  $H_2TiO_3$  adsorbs  $Li^+$  in LiCl solution well fits the Langmuir equation with monolayer adsorption.

Key words: Li<sup>+</sup> adsorbent; Li<sub>2</sub>TiO<sub>3</sub>; adsorption property; kinetic models; monolayer adsorption; TiO<sub>2</sub>; Li<sub>2</sub>CO<sub>3</sub>

# **1** Introduction

Traditional precipitation, solvent extraction and salting method [1,2] are not suitable for a small amounts of Li-containing sea water and salt lake brine on lithium extraction. A new separating technique [3,4] of alkali and alkaline metals with similar nature benefits from the inorganic separation material with ion function memory. At present, the study of lithium ionic sieve is mainly focused on manganese lithium ionic sieve [5-7], which exists in the disfigurement of few cyclic number and big dissolved loss etc. Titanium lithium ionic sieve has some remarkable advantages, such as less dissolved loss and stable structure. Li4Ti5O12 was synthesized by the sol-gel method [8,9] and the lithium ionic sieve was obtained after acid treatment. The pull-out rate of lithium reached 81.5%, while that of titanium ion was below 4.2%. The adsorptive capacity for lithium ion reached 42.30 mg/g.  $Li_2TiO_3$  was obtained via the solid phase synthesis method [10-12] with mixed crystal titanium dioxide (anatase content was 83.1%) as raw material and lithium ionic sieve was acquired after pickling. Its saturated adsorptive capacity came up to 28.76 mg/g. Li<sub>2</sub>TiO<sub>3</sub> had a special separation effect on lithium in the brine gas field with high calcium and magnesium but low lithium. It can be seen that the form of titanium dioxide used has a great influence on the adsorption performance of  $Li_2TiO_3$ , which was used as the lithium adsorbent precursor.

In this work,  $Li_2TiO_3$  was synthesized by a solidphase method with mixed crystal titanium dioxide. Then lithium adsorbent (H<sub>2</sub>TiO<sub>3</sub>) was obtained by pickling with hydrochloric acid. The structure characteristics and ion-exchange properties were studied by XRD, SEM, Li<sup>+</sup> adsorption isotherm, kinetics and adsorption measurement, respectively.

# 2 Experimental

The experimental technology process is shown in Fig. 1. The lithium adsorbent precursor was synthesized by a solid-phase reaction between  $TiO_2$  and  $Li_2CO_3$ . Prior to calcination, the mixture of  $TiO_2$  and  $Li_2CO_3$  was milled and blent with anhydrous alcohol as dispersant. Then it was dried at 100 °C for 2 h. Finally, the dried mixture was calcined at 850 °C for 24 h and pickled with hydrochloric acid. The adsorbent was used to adsorb lithium ion in solution, then it was regenerated with hydrochloric acid.

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Fig. 1 Flow chart of experimental process

# **3** Results and discussion

#### 3.1 Synthesis of lithium adsorbent precursor (Li<sub>2</sub>TiO<sub>3</sub>)

The XRD patterns of  $\text{Li}_2\text{TiO}_3$  synthesized under different lithium titanium ratios (*R*=2.00, 2.04, 2.10, 2.16) with  $\text{Li}_2\text{CO}_3$  and  $\text{TiO}_2$  are shown in Fig. 2. The results indicate the pure phase of  $\text{Li}_2\text{TiO}_3$  can be obtained under all ratios. The intensities of diffraction peaks increase with increasing the lithium titanium ratio, which indicates that the crystal shape is more complete under a higher lithium to titanium ratio.



**Fig. 2** XRD patterns of  $Li_2TiO_3$  synthesized with different titanium to lithium ratios

#### 3.1.1 Lithium to titanium ratio

The effect of lithium to titanium ratio (R= n(Li)/n(Ti), 2.00, 2.04, 2.08, 2.10, 2.14, 2.16) on lithium extraction and titanium dissolved loss rate is shown in Fig. 3. Under the same pickling conditions (0.25 mol/L HCl, 60 °C), lithium drawn out reduces with the increasing of *R*. The extraction rate of lithium is 85.62% when *R* is 2, but it is reduced to 77.87% at *R*=2.16. In contrast, the dissolved loss rate of titanium increases slowly with the increasing of *R*, which is 0.17% when *R* is 2 and it is increased to 0.34% at *R*=2.16. Figure 4 shows the effect of *R* on the adsorptive capacity. As can

be seen from Fig. 4 the adsorptive capacity decreases with an increase of R under the same pickling and adsorption conditions. The adsorptive capacity is 25 mg/g when R is 2 and decreases to 11.8 mg/g when Rincreases to 2.16. This indicates that the crystal structure of Li<sub>2</sub>TiO<sub>3</sub> becomes more complete and stable with the increase of R, which is consistent with that in Fig. 2. According to lithium extraction, titanium dissolution loss rate and adsorptive capacity, the optimum chemical ratio is chosen as 2.



**Fig. 3** Effects of lithium to titanium mole ratio on lithium extraction and titanium dissolved loss rate



Fig. 4 Effect of lithium to titanium mole ratio on adsorptive capacity

#### 3.1.2 Synthesis temperature

Figure 5 shows the effects of temperature on the XRD patterns of lithium adsorbent precursor obtained under the conditions of lithium to titanium ratio of 2 and calcining time of 24 h. The pure phase of  $Li_2TiO_3$  can be synthesized from 550 °C to 1050 °C. All diffraction peak intensities increases with the synthesis temperature increased from 550 °C to 850 °C, which illustrates that the crystal structure of  $Li_2TiO_3$  becomes more complete with increasing the temperature. The results show that all the diffraction peak intensities become weak gradually



Fig. 5 XRD patterns of  $Li_2TiO_3$  synthesized at different temperatures

when the temperature is higher than 850 °C. According to Refs. [13–15], the single inclined crystal of  $Li_2TiO_3$  is converted into the cubic crystal when the temperature is higher than 1150 °C. It can be concluded that the structural change stage happened when the temperature is higher than 850 °C, which leads to a weaker diffraction peak intensity.

Figure 6 shows the effect of synthesis temperature on lithium extraction and titanium dissolved loss rate. Lithium extraction rate decreases with the increase of synthesis temperature under the same pickling conditions (0.25 mol/L HCl, 60 °C). The rates of lithium elicited are 88.31%, 85.62% and 56.21% at synthesis temperatures of 550, 850 and 1050 °C, respectively. The titanium dissolved loss rate increases with the increase of synthesis temperature. The titanium dissolved loss rates are 0.15%, 0.17% and 1.16% at synthesis temperatures of 550, 850 and 1050 °C, respectively.

The lithium adsorbent adsorptive capacity shows little dependence on temperature in the range of 550-850 °C, as shown in Fig. 7. The adsorptive capacities are



Fig. 6 Effects of synthesis temperature on lithium extraction and titanium dissolved loss rate



Fig. 7 Effect of synthesis temperature on lithium adsorptive capacity

26.2 and 25 mg/g at 550 °C and 850 °, respectively. When the temperature is 1050 °C, the adsorption capacity decreases sharply to 4 mg/g. It can be concluded that the suitable synthesis temperature is between 550 °C and 850 °C by considering the lithium extraction rate, titanium dissolved loss rate and lithium adsorptive capacity comprehensively.

# 3.2 Preparation and characterization of lithium adsorbent (H<sub>2</sub>TiO<sub>3</sub>)

Lithium adsorbent (H<sub>2</sub>TiO<sub>3</sub>) was obtained when the lithium adsorbent precursor was treated with hydrochloric acid. Figure 8 shows the relationship between the lithium extraction and the extracting time. As can be seen from Fig. 8, the rate of lithium extracted reached 83.64% when Li<sub>2</sub>TiO<sub>3</sub> was treated by pickling for 24 h. Then it increased slowly with the extension of time, so it reached 98.86% after 96 h. While the content of the titanium ion in solution was almost zero through spectrophotometry method, which suggests that titanium is almost insoluble loss in the pickling process.

Figure 9 shows XRD patterns of  $Li_2TiO_3$ ,  $H_2TiO_3$  before and after adsorbing  $Li^+$ . Figure 9(a) shows XRD



Fig. 8 Variation of Li<sup>+</sup> extraction rate with reaction time



**Fig. 9** XRD patterns of  $Li_2TiO_3$  (a),  $H_2TiO_3$  before (b) and after (c) adsorbing  $Li^+$ 

patterns of pure monoclinic crystal of Li<sub>2</sub>TiO<sub>3</sub> (the lattice constant: a=0.5069 nm, b=0.8799 nm, c=0.9759 nm, JCPDS 33—831). The pattern in Fig. 9(b) shows that the diffraction peak shifts to right and the strength weakens significantly compared with the pattern in Fig. 9(a). The diffraction peaks of pattern become wide. All of the changes indicate that hydrogen ions (radius is about 0.0012 nm) exchange with lithium atoms (radius is about 0.076 nm) when Li<sub>2</sub>TiO<sub>3</sub> is treated with acid. The crystal interplanar spacing becomes narrow and the grains become small after treatment. It can be seen that the XRD pattern in Fig. 9(c) is alike with that in Fig. 9(b), which suggests that the structure does not change much after absorption.

Figure 10 shows the SEM images of  $Li_2TiO_3$ ,  $H_2TiO_3$  before and after adsorbing  $Li^+$ . It can be seen from Fig. 10,  $Li_2TiO_3$  obtained by solid-phase synthesis method is comparatively uniform, with the particle size of 1–2 µm. Figures 10(b) and (c) show the particles with some irregular crackles.

#### 3.3 Adsorptive properties

#### 3.3.1 Saturated adsorptive capacity

Figure 11 shows the adsorptive capacity of lithium adsorbent (H<sub>2</sub>TiO<sub>3</sub>) in LiOH solution of 694.1 mg/L Li<sup>+</sup>, LiCl solution of 282.5 mg/L Li<sup>+</sup> and 87.5 mg/L Li<sup>+</sup>. The results show that the adsorptive capacity increases with the increase of time in LiOH or LiCl solution. The adsorptive capacity increases quickly in the first 24 h and then increases slowly with prolonging time. Finally, it reaches a plateau after 192 h. The adsorptive capacities are 39.8, 30.9 and 28.63 mg/g in deferent solutions described above, respectively. The results indicate that the absorbent has strong adsorption ability to lithium in the alkaline solution. The adsorption reaction is as follows: H<sub>2</sub>TiO<sub>3</sub>+Li<sup>+</sup> $\rightarrow$ Li<sub>2</sub>TiO<sub>3</sub>+H<sup>+</sup>. H<sup>+</sup> was released and



Fig. 10 SEM images of  $Li_2TiO_3$  (a),  $H_2TiO_3$  before (b) and after (c) adsorbing  $Li^+$ 



Fig. 11 Variation of adsorptive capacity with time

 $OH^-$  was consumed constantly when lithium ion in the solution was adsorbed constantly. The adsorptive capacity increased slowly until the adsorption balance reached with the extension of time. Thus the adsorptive capacity in LiOH solution was more than that in LiCl solution, which was also concluded by AYDIN et al [16] and MARTIN et al [17].

## 3.3.2 Adsorption dynamics

The lithium generally exists in the form of LiCl in saline brine, so the adsorption dynamics that the adsorbent adsorbed in LiCl solution with different concentrations was investigated. There were many reports about the adsorption dynamics research of adsorbent for metal ions. At present, the pseudo-first-order (equation 1) and pseudo-second-order (equation 2) kinetic models are widely used to study the adsorption mechanism and determine the rate constant of adsorption process [18–20]:

$$\lg(q_e - q_t) = \lg q_e - \frac{k_{\rm ad}}{2.303} \times t \tag{1}$$

$$\frac{t}{q_t} = \frac{1}{kq_e^2} + \frac{1}{q_e} \times t \tag{2}$$

where  $q_e$  and  $q_t$  are the absorbent adsorptive capacities to Li<sup>+</sup> at adsorption equilibrium and any time *t*, respectively;  $k_{ad}$  and *k* are the rate constants of the pseudo-first-order and pseudo-second-order kinetic models, respectively.

The curves b and c in Fig. 11 are made a linear fitting with the pseudo-first-order and pseudo-second-order dynamic equations, and the results are shown in Fig. 12 and Table 1. As shown in Fig. 12 and Table 1, the

linear correlation coefficient of the pseudo-second-order dynamic equation is 0.999, which is greater than that of the pseudo-first-order dynamic equation. Thus it can be concluded that the adsorption dynamics in LiCl solution is conformed to the pseudo-second-order kinetic model. Some important kinetic parameters can be calculated by the pseudo-second-order dynamic equation. For example, the rate constants at the two concentrations are 0.00574 and 0.0051 g/(mg·h), respectively. The equilibrium adsorptive capacities are 29.32 and 31.63 mg/g. The adsorptive capacities are fairly near 28.63, 30.9 mg/g according to Fig. 11, respectively. This further confirms the conclusion that the adsorption in LiCl solution conforms to the pseudo-second-order dynamic equation and the adsorption process is mainly a chemical adsorption [21].

#### 3.3.3 Adsorption isotherm

The experimental data were analyzed by the Langmuir and Freundlich models [22], the equations of which can be expressed as

$$\frac{\rho_{\rm e}}{q_{\rm e}} = \frac{1}{q_{\rm m}} \rho_{\rm e} + \frac{1}{K_{\rm L} q_{\rm m}} \tag{3}$$

$$\lg q_{\rm e} = \frac{1}{n} \lg \rho_{\rm e} + \lg K_{\rm F} \tag{4}$$

where  $\rho_e$  is the equilibrium concentration of Li<sup>+</sup> solution;  $q_e$  is the equilibrium adsorptive capacity of Li<sup>+</sup>;  $q_m$  is the theoretical maximum adsorptive capacity of Li<sup>+</sup>;  $K_L$  is the Langmuir empirical constant; *n* and  $K_F$  are the Freundlich constants indicating relative adsorptive capacity and adsorption rate, respectively.



Fig. 12 Pseudo-first-order (a) and pseudo-second-order (b) kinetic plots for  $Li^+$  adsorption at different  $Li^+$  concentrations

Table 1 Kinetic parameters for Li<sup>+</sup> adsorption at different concentrations

$ ho_{\mathrm{Li}}^{+}/(\mathrm{mg}\cdot\mathrm{L}^{-1})$	$q_{\rm e}({\rm exp.})/({\rm mg}\cdot{\rm g}^{-1})$	Pseudo-first-order			Pseudo-second-order		
		$k_{\rm ad}/{\rm h}^{-1}$	$q_{\rm e}$ (theor.)/(mg·g <sup>-1</sup> )	$R^2$	$k/(g \cdot mg^{-1} \cdot h^{-1})$	$q_{\rm e}$ (theor.)/(mg·g <sup>-1</sup> )	$R^2$
87.5	28.63	0.01988	11.89	0.9217	0.00574	29.32	0.9997
282.5	30.90	0.01974	13.35	0.9477	0.0051	31.63	0.9992

The equilibrium concentration of  $Li^+$  and adsorptive capacity of adsorbent in LiCl solution of different concentrations were fitted linearly with Langmuir and Freundlich models. The results are shown in Fig. 13 and Table 2. The linear correlation coefficient of Langmuir model reaches 0.9984, which is much greater than that of Freundlich model. This indicates the adsorption of absorbent for Li<sup>+</sup> conforms to Langmuir model. It is a monolayer adsorption and the maximum absorption capacity is 37.01 mg/g.



**Fig. 13** Langmuir (a) and Freundlich (b) isotherms in LiCl solution of different concentrations

**Table 2** Type and parameters of isothermal adsorption of  $Li^+$ -adsorbent

	Langmuir		Freundlich		
$q_{ m m}/$ (mg·g <sup>-1</sup> )	$K_{\rm L}/$ (L·mg <sup>-1</sup> )	$R^2$	n	$K_{\rm F}/$ (L·g <sup>-1</sup> )	$R^2$
37.01	0.15333	0.9984	25.3229	28.5351	0.8814

3.3.4 Peculiarity of selective adsorbent to lithium ion

The lithium absorbent was placed in the salt lake brine to make a cycle experiment and carry a study on the separation properties of absorbent for the main metal ions in it. Table 3 lists the separation coefficients of lithium ion to several main metal ions in brine. As can be seen from Table 3, the adsorbent has better separation properties of Li<sup>+</sup> to Na<sup>+</sup>, K<sup>+</sup> and Mg<sup>2+</sup>, but the separation coefficient is not very large, which is related with the adsorption time and the nature of brine. In the brine, the content of Li<sup>+</sup> is low, while that of Na<sup>+</sup>, K<sup>+</sup> or Mg<sup>2+</sup> is very high. The separation coefficient becomes more and more with the cycle carrying. This indicates that the increase of cycle times is beneficial to the separation of Li<sup>+</sup> to K<sup>+</sup>, Na<sup>+</sup> and Mg<sup>2+</sup> in salt lake brine. The separation coefficient of lithium to magnesium reaches 102.40 at the 8th adsorption, which can be a good separation of lithium and magnesium ions in salt lake brine.

 Table 3 Separation coefficients of lithium ion to several main

 metal ions in brine

Designation	Separation coefficient				
Designation	${\alpha_{\rm K}}^{ m Li}$	$\alpha_{ m Na}^{ m Li}$	${a_{\mathrm{Mg}}}^{\mathrm{Li}}$		
1st adsorption	16.36	15.38	12.87		
5th adsorption	29.51	26.97	27.75		
8th adsorption	30.98	29.46	102.40		

# **4** Conclusions

1) A single crystal phase of  $Li_2TiO_3$  can be synthesized by solid method using titanium dioxide and lithium carbonate as raw materials. Optimization preparation conditions of metatitanate lithium precursor are: lithium to titanium ratio of 2, synthesis temperature of 850 °C and synthesis time of 24 h.

2) Lithium adsorbent (H<sub>2</sub>TiO<sub>3</sub>) can be obtained after pickling Li<sub>2</sub>TiO<sub>3</sub> with hydrochloric acid. The extraction ratio of Li<sup>+</sup> from Li<sub>2</sub>TiO<sub>3</sub> reached 98.86%, and the rate of titanium dissolved loss was only 0.17%.

3) Lithium adsorbent  $(H_2TiO_3)$  has an excellent adsorption ability to Li<sup>+</sup>. The equilibrium adsorptive capacity in LiOH solution containing 694.1 mg/L Li<sup>+</sup> reached 39.8 mg/g.

4) The adsorption process that  $H_2TiO_3$  adsorbs  $Li^+$ in LiCl solution conformed to the pseudo-second-order dynamic equation, which shows that the adsorption process is mainly chemical adsorption. What's more, the adsorption process also conformed to Langmuir model, which shows that the adsorption process is monolayer absorption.

5) The separation coefficient of lithium to magnesium reaches 102.4 at the 8th adsorption, which can be a good separation of lithium and magnesium ions in salt lake brine.

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# 锂离子吸附剂(H<sub>2</sub>TiO<sub>3</sub>)的合成及吸附性能

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摘 要:选取TiO<sub>2</sub>为钛源、Li<sub>2</sub>CO<sub>3</sub>为锂源,采用高温固相法合成锂吸附剂前躯体Li<sub>2</sub>TiO<sub>3</sub>,并探讨锂钛比、焙烧 温度、焙烧时间等因素对合成Li<sub>2</sub>TiO<sub>3</sub>性质的影响。将Li<sub>2</sub>TiO<sub>3</sub>用一定浓度的盐酸酸洗脱锂后制得偏钛酸型锂吸附 剂H<sub>2</sub>TiO<sub>3</sub>,酸洗过程中锂的抽出率达到98.86%,而离子筛中的钛溶损却很小。采用XRD和SEM等分析手段对 TiO<sub>2</sub>、Li<sub>2</sub>TiO<sub>3</sub>和H<sub>2</sub>TiO<sub>3</sub>及其吸附锂后的样品进行表征。最后应用伪一级和伪二级动力学方程对H<sub>2</sub>TiO<sub>3</sub>的吸附性 能进行研究,并对吸附过程进行拟合从而计算相应的速率常数。结果表明:H<sub>2</sub>TiO<sub>3</sub>对锂离子具有较大的吸附能力, 吸附过程符合伪二级动力学方程,表明吸附过程主要为化学吸附;在LiCl溶液中的吸附平衡数据符合Langmuir 等温吸附方程,表明吸附过程为单层吸附。

关键词: 锂离子吸附剂; Li<sub>2</sub>TiO<sub>3</sub>; 吸附性能; 动力学模型; 单层吸附; TiO<sub>2</sub>; Li<sub>2</sub>CO<sub>3</sub>

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