Reaction kinetics of roasting high-titanium slag with concentrated sulfuric acid

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Abstract: A novel method of roasting high-titanium slag with concentrated sulfuric acid was proposed to prepare titanium dioxide, and the roasting kinetics of titania was studied on the basis of roasting process. The effects of roasting temperature, particle size, and acid-to-ore mass ratio on the rate of roasting reaction were investigated. The results showed that the roasting reaction is fitted to a shrinking core model. The results of the kinetic experiment and SEM and EDAX analyses proved that the reaction rate of roasting high-titanium slag with concentrated sulfuric acid is controlled by the internal diffusion on the solid product layer. According to the Arrhenius expression, the apparent activation energy of the roasting reaction is 18.94 kJ/mol.

Key words: roasting kinetics; high-titanium slag; concentrated sulfuric acid; titania

1 Introduction
Titanium dioxide is an important inorganic chemical material, and is extensively used in white pigment, paper, plastics, rubbers, porcelain, and fibers, etc [1–4]. The main processes for the production of titanium dioxide are sulfate process and chloride process. In the sulfate process, titanium sulfate solution is subsequently hydrolyzed in highly acidic solutions, and then the precipitate of hydrous titanium oxides is obtained. The comprehensive management of waste acid and by-product of copperas are the most fatal weakness in the sulfate process [5–8]. On the other hand, the chloride process requires a feedstock of high TiO2 grade and must satisfy the content limit of MgO+CaO less than 1.5%. Moreover, it is a high energy consuming process [9–11]. All the above-mentioned shortcomings prevent the development of the chloride process in industry. Therefore, it is significant to put forward novel technique and method for the production of titanium dioxide.

The reserve volume of vanadium–titanium magnetite resources is sufficient in Panxi region of Sichuan Province, China. In the course of the smelting of pig iron, titanium is discharged into the blast furnace slag, which pollutes the environment seriously [12–15]. High-titanium slag contains a large number of valuable metals, such as silicon, aluminium, calcium. Therefore, it is very meaningful to realize the comprehensive utilization of high-titanium slag. The procedure of extracting titanium dioxide from high-titanium slag can reduce a step of elimination of copperas and therefore the energy consumption is decreased consequently. It is apparent that the productivity is promoted and the pollution is relieved [16–18]. Hence, the high-titanium slag is adopted as the basic high-quality raw materials in titanium industry, which has a certain economic value.

The presented method of roasting high-titanium slag with concentrated sulfuric acid in this work has the advantages of saving time, low consumption of acid and high acidolysis rate. The more important term is that the waste sulfuric acid can be recycled. The effects of reaction conditions, such as roasting temperature, particle size and acid-to-ore mass ratio, on the reaction rate of roasting high titanium slag with concentrated sulfuric acid were considered sufficiently and analyzed. Furthermore, the appropriate kinetic equation and the rate-controlling step of roasting reaction were derived. Finally, the reaction mechanism was discussed in detail.

2 Experimental

2.1 Materials
Titanium slag after crushing and ball milling...
was used in the experiment. The chemical compositions of the high-titanium slag are listed in Table 1. The main component of titanium slag is TiO$_2$, and its content is 48.65%. All the chemical reagents were of analytical grade, and deionized water was used throughout the experimental process.

Table 1 Chemical compositions of high-titanium slag (mass fraction, %)

<table>
<thead>
<tr>
<th></th>
<th>TiO$_2$</th>
<th>Al$_2$O$_3$</th>
<th>Fe</th>
<th>SiO$_2$</th>
<th>MgO</th>
<th>CaO</th>
<th>Mn</th>
</tr>
</thead>
<tbody>
<tr>
<td>Mass fraction (%)</td>
<td>48.65</td>
<td>14.30</td>
<td>3.71</td>
<td>17.55</td>
<td>7.50</td>
<td>5.70</td>
<td>0.77</td>
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The mineralogical phases of the high-titanium slag were investigated by X-ray powder diffraction. The XRD pattern shown in Fig. 1 indicates that the main crystalline phases of the high-titanium slag are anosovite solid solution of magnesium and iron (Mg$_{0.5}$Fe$_{0.5}$)Ti$_2$O$_5$ and complex silicate phase Al$_2$Ca(SiO$_4$)$_2$. FeO and MgO in titanium slag are beneficial to the increase of acidolysis rate of titanium slag.

Fig. 1 XRD pattern of high titanium slag

2.2 Procedure

Experiments were performed in a resistance wire heating furnace. The concentrated sulfuric acid and high-titanium slag were homogeneously mixed in the porcelain crucibles. Then the crucibles were put into the resistance wire heating furnace and heated. When the temperature reached the predetermined temperature, we began to activate the timing device. The porcelain crucible was taken out at specified time and cold water was added quickly in order to stop the reaction immediately, with free access to air in the whole process. The temperature of the resistance wire heating furnace was controlled by a programmable temperature controller, with a precision of ±1 °C. The roasting product was leached by water (leaching conditions: temperature 70 °C, solid-to-liquid ratio 1:4, and stirring time 1 h). The extraction rate of TiO$_2$ was determined by the ammonium ferric sulfate dodecahydrate titration. The calculating formula of the extraction rate of TiO$_2$ is expressed as

$$x(\text{TiO}_2) = \frac{m'(\text{TiO}_2)}{m(\text{TiO}_2)}$$

where $x(\text{TiO}_2)$ is the extraction rate of TiO$_2$; $m'(\text{TiO}_2)$ is the mass of TiO$_2$ in the filtrate; $m(\text{TiO}_2)$ is the total mass of TiO$_2$ in high-titanium slag.

3 Results and discussion

3.1 Effect of temperature

The influence of roasting temperature on the reaction rate of high-titanium slag with concentrated sulfuric acid was investigated in the temperature range of 250–310 °C, with acid-to-ore mass ratio of 2:1 and particle size of 45–48 μm. Figure 2 shows that temperature has a significant effect on the reaction rate of roasting high-titanium slag. The extraction rate of TiO$_2$ increases rapidly with the increase of temperature.

Fig. 2 Relationship between extracting rate of TiO$_2$ and time at different temperatures

In order to determine the kinetic parameters and rate-controlling step for roasting high-titanium slag with concentrated sulfuric acid, the experimental data presented in Fig. 2 were analyzed on the basis of the shrinking-core model. The experimental data were substituted into the Crank–Ginsting–Braunshtein’s kinetic equation [19–22]:

$$1+2(1-x)-3(1-x)^{2/3}=Kt$$

where $x$ is the extraction rate of TiO$_2$; $K$ is the apparent rate constant; $t$ is the reaction time. The corresponding relationship between the value of $1+2(1-x)-3(1-x)^{2/3}$ and the roasting time $t$ is described in Fig. 3, which shows that the linear relationship between $1+2(1-x)-3(1-x)^{2/3}$ and roasting time $t$ is significant. The results indicate that
the reaction rate is fitted to the Crank–Ginsting–
Braunshtein’s kinetic equation, which proves that the reaction rate is controlled by the internal diffusion on the solid product layer in the roasting process.

According to the Arrhenius expression:

$$
\ln K = \ln A - \frac{E}{RT}
$$

(3)

where $K$ is the rate constant, $A$ is the frequency factor, $E$ is the apparent activation energy, $R$ is the mole gas constant and $T$ is the thermodynamic temperature. The corresponding relationship between $\ln K$ and $1/T$ is revealed in Fig. 4, where the approximation of the apparent activation energy can be obtained from the slope of the plotted straight line ($E = 18.94$ kJ/mol). The result verifies that the reaction rate is controlled by the internal diffusion.

3.2 Effect of particle size

The influence of particle size on the reaction rate of roasting high titanium slag with concentrated sulfuric acid was studied (the roasting temperature was 310 °C and the acid-to-ore mass ratio was 2:1), using the three particle size fractions: 160–180, 75–80, 45–48 μm, respectively. The results presented in Fig. 5 show that the particle size of high-titanium slag has a significant effect on the extraction of TiO$_2$. The extraction rate of TiO$_2$ increases with the decrease of particle size because the decrease of particle size increases both the specific surface of the titanium slag and its reactivity. The experimental data are substituted into the Crank–Ginsting–Braunshtein’s kinetic equation: $1+2(1-x)-3(1-x)^{2/3} = Kt$.

According to the experimental data in Fig. 5, the plots of $1+2(1-x)-3(1-x)^{2/3}$ vs time $t$ are presented in Fig. 6. The linear relationship between $1+2(1-x)-3(1-x)^{2/3}$ and roasting time $t$ is significant. The results further indicate that the roasting process is controlled by the internal diffusion on the solid product layer.

3.3 Effect of acid-to-ore mass ratio

The influence of acid-to-ore mass ratio on the reaction rate of roasting high-titanium slag with concentrated sulfuric acid was studied (the roasting temperature was 310 °C and the range of particle size
was 45−48 μm), using three acid-to-ore mass ratios: 1.9:1, 2.0:1 and 2.1:1, respectively. The results in Fig. 7 show that the extraction rate of TiO₂ increases with the increase of acid-to-ore mass ratio. The experimental data are substituted into the Crank−Ginsting−Braunshtein’s kinetic equation. The corresponding relationship between the value of 1+2(1−x)−3(1−x)²/³ and the roasting time t is described in Fig. 8, which shows that there is a good linear correlation between the above two variables. The results further indicate that the roasting process is controlled by the internal diffusion on the solid product layer.

\[ 1+2(1-x) - 3(1-x)^{2/3} = 0.4946\exp\left(-\frac{18940}{RT}\right)t \]  

### 4 Analysis of roasting reaction mechanism

The main reaction of the roasting high-titanium slag with concentrated sulfuric acid could be described as follows:

\[ 2(Mg_{0.5}Fe_{0.5})Ti_2O_5 + 6H_2SO_4 = 4TiOSO_4 + MgSO_4 + FeSO_4 + 6H_2O \]  

\[ Al_2Ca(SiO_4)_2 + 4H_2SO_4 = Al_2(SO_4)_3 + CaSO_4 + 2SiO_2 + 4H_2O \]

The scanning electron microscopy (SEM) was employed to investigate the change of morphology and elemental composition of titanium slag and the residue. From the results given in Fig. 9, the titanium slag is granular and high-density. The surface of the residue is rough after the reaction and the morphology of titanium slag is destroyed.

![Fig. 9 SEM images of high-titanium slag (a) and residue (b)](image)

Based on the above experiments, it can be concluded that the kinetic experimental data are fitted to the Crank−Ginsting−Braunshtein’s kinetic equation under all the experimental conditions. The reaction rate of roasting high titanium slag with concentrated sulfuric acid is controlled by the internal diffusion on the solid product layer. In the range of experimental temperature, the kinetic equation of roasting process can be described as follows:

\[ 1+2(1-x) - 3(1-x)^{2/3} = 0.4946\exp\left(-\frac{18940}{RT}\right)t \]
2.140%, Ca 5.346%. According to the analysis results, the main elements of the surface of the residue are Si and Ca, while Ti content reduces greatly, which proves the existence of a solid product layer.

According to the analysis results, the main elements of the surface of the residue are Si and Ca, while Ti content reduces greatly, which proves the existence of a solid product layer.

The reaction of roasting high-titanium slag with concentrated sulfuric acid is a liquid–solid reaction, which can be analyzed with the shrinking-core model under the assumption that the titanium slag is homogeneously spherical solid phase. The reaction is carried out in the solid particle surface. The reaction can generate not only the titanium ions, but also silica and calcium sulfate solid. The molecules of sulfuric acid must pass through the film formed by solid product to diffuse into the surface of titanium slag particles which do not participate in the reaction and react with titanium slag. So it can be concluded that the rate of roasting reaction is controlled by the internal diffusion on the solid product layer.

5 Conclusions

1) The reaction kinetics of roasting high-titanium slag with concentrated sulfuric acid was studied. The results of the kinetic experiment, SEM and EDAX analysis prove that the roasting kinetics is fitted to a shrinking core model with the reaction rate controlled by the internal diffusion on the solid product layer.

2) The apparent activation energy of the roasting reaction is 18.94 kJ/mol, which accords with the range of diffusion controlled processes.

3) The reaction rate satisfies the Crank–Ginsting–Braunshtein’s kinetic equation. The roasting kinetic equation can be described as follows:

$$1+2(1-x)-3(1-x)^{2/3} = 0.4946\exp\left(-\frac{18940}{RT}\right)$$

References


浓硫酸焙烧高钛渣的反应动力学

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摘 要：提出一种新方法，利用浓硫酸焙烧高钛渣提取二氧化钛，并在焙烧工艺的基础上研究焙烧反应动力学。考察焙烧温度、粒度以及酸矿比对反应速率的影响。结果表明，焙烧反应符合未反应核收缩模型。动力学实验数据、SEM 和 EDAX 结果分析表明，用浓硫酸焙烧高钛矿渣的反应受通过固体产物层的内扩散控制。Arrhenius 方程得到焙烧反应的表观活化能为 18.94 kJ/mol。

关键词：焙烧动力学；高钛渣；浓硫酸；二氧化钛

(Edited by Hua YANG)